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**Ref.: Revision MS JCA-16-1434**

Dear Editor,

I am pleased to send you our response to reviewer comments on **MS JCA-16-1434**.

In this point-by-point response, for your convenience, our answers are reported in italic just after each comment of reviewers written in quotation marks.

At the end of the rebuttal letter, a copy of the paper where all changes made in the MS are clearly evidenced (in red: added text; ~~strikeout~~: deleted text) has been included.

Thank you in advance for your time and cooperation.

With best regards,

Alberto Cavazzini  
Francesco Gasparrini

## Point-by-point response to reviewer comments

*In this point-by-point response, line numbers indicating changes made to the MS refer to the revised version of the MS where changes are enlighten (in red: added text; strikeout: deleted text). This version is appended at the end of rebuttal letter.*

### Reviewer-1

“All what ref. 9 mentions about chiral SPS materials is "2.4. Selector immobilization on fused core HALO materials (subsection title) and the text "The HALO silica material was modified similarly to our previously published protocol [47]." Perhaps these authors even did not on purpose synthesize SPS-based CSP, did not study it and did not mention even single word about them in the entire discussion. Thus, when citing ref. 9 as very first work in this field the authors at least have to remark that this manuscript does not discuss these materials as such at all. The authors definitely understand who I am. Therefore, I do not have any problem to disclose my name to them. Fairness is the major issue in the scientific publishing and must be respected by everyone. Please avoid distributing wrong credits and give that to real pioneers. Since you by yourself have pioneered many interesting innovations in our common field of scientific interest following my concept above is very important for yourself.”

*This point was well taken. The reviewer is absolutely right. We apologize with him/her, as we also do believe that fairness is most important in science. The MS was accordingly changed (ll. 31-32). Hopefully, we have now given right credits to those who deserve it.*

“Another example of wrong interpretation the literature is given in lines 50-51. I kindly ask the authors to carefully read ref. 10 in order to understand who for the first time recognized the advantage of SPS-based CSPs from the viewpoint of resolution per unit time discussed in these lines. Daniel Armstrong behaved unethical way declaring this as his own finding and the authors of the present manuscript propagate that wrong behavior. Prof. Gasparrini is very careful person and I am really very much surprised for his overlooking on this regard.”

*See our previous comment. Also in this case, the MS has been accordingly modified (ll. 34-38).*

“Line 59 and elsewhere in the text: writing trans(*italic*)-stilbene oxide in this way seems to be better.”

*The advice was well taken and the text was modified.*

“In the Experimental part the locations of USA companies must be cited according to the format "city, state, country" and the companies from other countries "city, country".”

*The advice was well taken and locations were added in the Experimental part.*

“In line 108 "Pirkle and co-workers" sounds better.”

*OK (see l. 116).*

“Line 211 and elsewhere in the text. There are quite many passages written in personal style. Rewriting these to impersonal style is recommended.”

*The advice was well taken and, accordingly, the text was modified where needed.*

“Ref. 12 is incorrect. It can be replaced with ref. 47.”

*The reviewer is right. Ref. 12 was corrected and ref. 47 was removed. Bibliographic references were accordingly updated*

## Reviewer-2

“Abstract, Line 6: Add  $\mu\text{m}$  after 2.6 in describing the SPPs.”

*The reviewer is right: “ $\mu\text{m}$ ” was added after 2.6.*

“Lines 13-17: I commend the authors for this statement as they have avoided the common argument of “lower RSD values” that many companies use as a key reason for good SPP performance in the A-term. While the hypothesis they discuss here may not necessarily be correct either (and clearly state as such), it tends to be in line with general observations and suggestions in a number of other recent publications.”

*Even though this point clearly needs additional experimental and theoretical work to be definitely answered, recent investigation is inclined to recognize particle roughness as one of the most important features.*

“Lines 35-44: In terms of the discussion on the limited performance of chiral SPPs in capillary columns, this observation may not be limited to only chiral stationary phases but core-shell morphologies in general. In a 2015 paper on the comparison of 5  $\mu\text{m}$  FPPs and SPPs in capillary columns (DOI: 10.3390/chromatography2030502), an exhaustive list of SPPs in capillary columns up to that point was provided (references 22-28 in said paper). It may not necessarily be the chiral phase that causes the issue, but rather differences in the wall effect (that has a bigger impact in capillary LC than it does in 1-4.6 mm bore columns) between SPPs and FPPs as performance also suffered in reversed phase C18 SPPs. Thus, in addition to the suggestion of difficulties of packing chiral phases mentioned here (Lines 42-43) it may be beneficial to note the overall difficulty in getting good SPP columns at the capillary scale. A more recent paper (DOI: 10.1016/j.chroma.2015.10.013) on packing SPPs in capillaries at higher slurry concentrations gave the best reported efficiencies for such columns to date. This further supports potential reasoning as to wall effects playing a role in differences between SPPs and FPPs in capillaries as high slurry concentrations tend to reduce wall effects.”

*We thank the reviewer for this observation. The revised MS was modified to include these observations (see ll. 45-50). Bibliographic references suggested by the reviewer were added (new Refs. 13-19). Bibliography was accordingly updated.*

“Lines 75-106: Between the article, the figure captions, and the supporting information, it is still not fully clear which LC was used for which section. I am led to believe that the Ultimate 3000 was used for most of the studies and that the Acquity was only used for the fast separations on the 1 cm column. Is this even correct?”

Please add a statement clarifying what instrumentation was used for what data in both the section on 'van Deemter curve measurements' and in the relevant figure captions (Figure S2 is a good example that should be used elsewhere).”

*We agree that this information was not clearly given. We apologize for that and we thank the reviewer for his/her careful reading of MS. The suggestion of the reviewer was accepted. In the revised MS (both in the experimental section, ll. 82 and 139-140, and in the figure captions) this information is now clearly given.*

“Lines 110-116: As a key part of this manuscript is comparing different stationary phases that are coated with a chiral phase, the results of the coating process in terms of loadability should be described more in-depth for reader understanding. Please include information on how you calculated the values in Table 1 from the elemental analysis or cite a previous paper where such calculations are detailed. Also, more details on the column packing process should be provided to the reader or a previous citation from the group that describes their protocol should be included.”

*A detailed description on how values from elemental analysis were calculated could be found in ref. 30. Even though this reference was already present in the first version of the MS, we added a sentence to explain that readers can find there all the information to perform the calculations see l. 122).*

*More details on the packing process were also added (see ll. 125-129).*

“Line 150: Please cite a source for the physical data related to the viscosity of THF.”

*Accordingly, ref. 35 was added.*

“Line 175-177 (and 375-376): There is another recent Armstrong article not cited in this manuscript (DOI: 10.1016/j.chroma.2014.09.010) where the results in Table 1 (specifically the 3  $\mu$ m FPP and the 2.7  $\mu$ m SPP) do not follow this same trend. Do those different results based on a different CSP suggest one of the listed possible reasons for this difference in binding over another? Please address.”

*We thank the reviewer for this observation. We admit that we were not aware about that. The information is very important in the context of this work. Not only the reference to this paper was added to the MS, but the text of the paper was changed to account for this. (see ll. 186-190)*

“Line 183: Remove 'relationship between'.”

OK

“Line 193: The last part of this sentence ("the larger being the efficiency, the higher the resolution") should instead read something like "with higher efficiencies giving better resolution".”

*The advice was well taken and the text was modified (see l. 214).*

“Lines 214-221: This section is very confusing and needs to be rewritten. First, "in spite of the highest density of chiral selector" is true for one factor of bonding density, but the overall much larger surface area for FPPs can outweigh this factor. In that case, the alpha value differences for the FPPs would likely have a bigger difference than in the SPPs which would give higher resolution. Also, when comparing the FPPs, not only is it column length but also particle diameter that would play a role in the measured efficiency that would affect the calculated resolution.”

*We thank the reviewer for this observation. Indeed, he/she is correct. Accordingly, the discussion has been modified to include these points (ll. 239-243).*

“Line 238: The data used to make the point about "less efficient packing" actually suggest "less dense packing" and the sentence should be changed to reflect that as packing density does not necessarily correlate with efficiency.”

*The advice was well taken and the text was modified (see ll. 263-265).*

“Lines 265-267: Based on the flow rates at those given pressures, what would the expected power generated (W/m) be? Do those values exceed the Gritti/Guiochon standard value of 4 W/m for loss in efficiency due to radial temperature gradients?”

*Yes, they do. For instance, at  $u_{int} = 0.8$  and  $1.0$  cm/s, frictional power of respectively 20.2 and 30.9 W/m can be easily calculated.*

“Line 289-291: The sentence regarding relating eddy dispersion and literature data is very confusing.”

*Thank you for reporting this. This part of the MS was modified (ll. 316-320). Hopefully now it is clearer.*

“Lines 296-297: What is meant by "time needed for bed consolidation"? Time needed to fill the packed bed or time needed to flush at a higher pressure to compress the bed? Also, in the experimental section it was stated that the columns are packed up to 1000 bar. What pressure were the columns actually run at? For columns run with the Acquity, the pressure limit is 1000 bar, so columns packed at 1000 bar might not be stable there (as a higher packing pressure than what will be used for column use is required for stable beds).”

*The time needed for bed consolidation in this paper is the time needed to compress the bed at high pressure flushing. This has been specified in the revised MS (ll. 325-326).*

*As for the comment about maximum pressure of packing vs. maximum operation pressure, there are not problems. Indeed, maximum pressures at which columns were operated are:*

- (i) long columns, 4 ml/min: 245 bar (2.6  $\mu\text{m}$  SPP 150x4.6 mm), 460 bar (1.8  $\mu\text{m}$  FPP 100x4.6 mm), 284 bar (2.5  $\mu\text{m}$  FPP 150x4.6 mm) at 4 mL/min;*
- (ii) short columns, 8 ml/min: 260 bar (2.6  $\mu\text{m}$  SPP 10x4.6 mm), 470 bar (1.8  $\mu\text{m}$  FPP 10x4.6 mm) and 690 bar (1.8  $\mu\text{m}$  FPP 10x3.0 mm).*

“Lines 297-302: This is an extremely long sentence that needs to be broken into separate ideas or shortened. (Even if, undoubtedly, more investigation..., in particular..., the impression is..., i.e. ....).”

*The advice was well taken and the sentence was shortened (see ll. 328-333).*

“Line 335: Analysis time is decreased 30-50%, not gained.”

*The reviewer is right. The text was modified (see l. 366).*

“Lines 339-346 and Figure 4B: Figure 4B seems unnecessary as it just repeats data that is shown in Figure 4A and divides it. The numbers shown in 4B could easily be included in the caption for Figure 4 and then discussed in the text in the same way they already are with no information lost.”

*It is true that Figure 4B does not introduce much more information than Figure 4a. In any case, in our opinion it visually gives a much clearer idea of the concept than a sentence written in the figure caption as this reviewer suggests. In addition, thinking about editorial issues, it is not an entire figure that should be removed but only a part of a figure. We decided accordingly to keep Figure 4 in its original form.*



“Lines 347-364: The fast chiral separations demonstrated in this section (and Figure 5) are rather remarkable and one of the most interesting parts of the paper. As other work by the Armstrong group and others on high-speed chiral separations is already included throughout the articles, this might be a relevant spot to also mention recent results from the Belder group on these types of separations on microfluidic platforms (DOI: 10.1021/acs.analchem.5b00210). Also, all of these columns were 3-4.6 mm in diameter... Is there potential to reduce the diameter to 2.1 mm as a way to reduce the excessive flow rates that were used, especially if reductions in extra-column volumes can be made?”

*First, we thank the reviewer for his/her nice comment. The advice to include a reference to the paper by Belder et al. was accepted (new reference 56). As for the observation about 2.1 diameter column, the answer is yes, in principle there is this possibility (in the sense that it is not a big issue to pack columns with this format). However, with 2.1 mm I.D. very short column, there is a big impact from extra volume contribution that, we fear, will dramatically impact on the separation. We are working on that and we hope to have soon some data to present.*

“Line 397: 'possess' to 'possession'?”

*The reviewer is right. The text was modified.*

“In Figure S1, it says that the Acquity was modified to enable the use of 10 mm columns. However, in the text (Line 357) it says that the Dionex pump was employed. Please clarify what is the correct instrumentation used for these final studies (Figure 5 and Table 3).”

*We thank the reviewer for this observation. A statement clarifying the instrumentation used was added in the captions of Figure 5 and Table 3.*

“Figure caption clarifications: I would mention carbon tetrachloride as the dead time marker in the captions for Figures 1, 4, and 5 and TSO as the enantiomers that are being separated in the captions for Figures 4 and 5.”

*We thank the reviewer for this observation. Accordingly, captions of Figs. 1, 4 and 5 were modified.*

“Reference 14 needs to be updated.”

*The reviewer is right. Ref. 14 was updated.*

# Pirkle-type chiral stationary phase on core-shell and fully porous particles: are superficially porous particles always the better choice towards ultrafast high-performance enantioseparations?

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## Abstract

Pirkle-type Whelk-O1 chiral stationary phase (CSP) was prepared on 2.6  $\mu\text{m}$  superficially porous particles (SPPs). The chromatographic behavior of columns packed with this new CSP was compared with that of columns packed respectively with 1.8 and 2.5  $\mu\text{m}$  Whelk-O1 fully porous particles (FPPs). In the comparison, both thermodynamic and kinetic aspects were considered. Contrary to our initial expectations, chiral columns packed with 2.6  $\mu\text{m}$  SPPs were quasi-comparable to those packed with 2.5  $\mu\text{m}$  FPPs, apparently due to larger contributions to band broadening from both eddy dispersion and, especially for the second eluted enantiomer, adsorption-desorption kinetics. These findings raise the question if SPPs, in spite of the undeniable advantages of their morphology to speed up mass transfer, are always the best choice for high-efficient ultrafast chiral separations. The last part of the work focuses on the use of short columns (10 mm long) and very high flow rates to realize the separation of the enantiomers of *trans*-stilbene oxide (TSO) in normal phase mode in less than one second.

**Keywords:** Whelk-O1 superficially porous chiral stationary phase; ultrafast

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## 1. Introduction

Last generation superficially-porous particles (SPPs) [1, 2], referred to also as core-shell, fused-core or solid-core particles, are made of a non-porous fused silica core surrounded by a porous shell, whose volume is usually 60-75% of particle volume. In terms of mass transfer, core-shell structure offers some advantages over that of a fully porous particle (FPP) since the contributions to band broadening from both the longitudinal diffusion due to the relaxation of axial gradient concentration along the column (the so called *B*-term of the van Deemter equation) and the solid-liquid mass transfer resistance due to the diffusion across the particle (*C*-term of the van Deemter equation) are reduced by the presence of the inaccessible core. In addition, columns packed with  $C_{18}$ -SPPs have been demonstrated to be extremely efficient also thanks to the very low eddy diffusion, which comes from flow unevenness in the interstitial zone of the column (*A*-term of the van Deemter equation) [3–5]. Even though the explanation of the low *A*-term for columns packed with  $C_{18}$  SPPs remains to a large extent unknown, the most accepted hypothesis is that roughness of core-shell particles limits particle slipping after releasing the high pressure employed for the preparation of the packed bed by slurry-packing, therefore reducing radial bed heterogeneity [1, 2]. The reason of the great success of SPPs is that they have provided a reasonable compromise between two opposite tendencies. Indeed, the tendency to improve analytical throughputs by means of columns packed with smaller and smaller particles and reduced dimensions is limited by instrumental factors, such as the extremely high pressures needed to operate these columns at high flow rates, on the one hand, and the effect of system extra-column volume on peak broadening, on the other. As a matter of fact, columns packed with  $2.7 \mu\text{m}$  SPPs are able to provide essentially the same efficiency as columns packed with sub  $2\text{-}\mu\text{m}$  FPPs (keeping constant column dimensions and experimental conditions), but at operating pressures similar to those of columns packed with  $3 \mu\text{m}$  FPPs [6, 7].

27 Surprisingly, the employment of SPPs in chiral chromatography is relatively recent  
28 [8]. The first work describing the use of SPPs in chiral HPLC dates 2011, when Lindner  
29 and coworkers prepared [9] a cinchona alkaloid based anion exchanger CSP by using 2.7  
30  $\mu\text{m}$  fused-core particles as base material. The column was successfully employed for  
31 the enantioseparation of amide type amino acid derivatives, **even if the authors do not**  
32 **mention the possible advantages given by this typology of CSP.** Chankvetadze and al.  
33 [10] firstly compared the kinetic performance of CSPs prepared on polysaccharide-coated  
34 FPPs and SPPs. **They mentioned some of the benefits of chiral SPPs over their fully porous**  
35 **counterparts, such as an higher enantioselectivity at comparable content of chiral selec-**  
36 **tor, a limited dependence of plate height on mobile phase flow rate and a larger enan-**  
37 **tioresolution per analysis time, with obvious benefits for high-throughput screening of**  
38 **chiral compounds** [10]. By using 4.6 mm I.D.  $\times$  250 mm columns, they demonstrated that  
39 columns packed with SPPs outperform those packed with FPPs in terms of efficiency and  
40 speed of analysis. Fanali and coworkers [11, 12] employed the same polysaccharide-based  
41 chiral particles used in [10] to pack capillary columns (75  $\mu\text{m}$  I.D.  $\times$  25 cm) for nano-liquid  
42 chromatography and electrochromatography experiments. They report about the diffi-  
43 culty to efficiently operate these capillaries. They conclude that, without further optimiza-  
44 tion, this column format does not allow to reach useful efficiency for high-performance  
45 separation. Even if the authors do not discuss in detail the reason of the poor performance  
46 of these packed capillaries, **more than on the kinetic performance of particles themselves,**  
47 **in our opinion (see also later on in this paper) this could depends either** on the difficulty  
48 of efficiently packing chiral core-shell particles (and thus to the contribution of eddy dis-  
49 **persion to peak broadening) or on the overall difficulty in getting efficient SPP columns at**  
50 **the capillary scale, more than on the kinetic performance of particles themselves.** [13–19]

51 The most systematic work on the comparison between chiral FPPs and SPPs has been  
52 done by Armstrong's group [20–22]. With the aim of investigating the potential of chiral  
53 SPPs for ultrafast enantioseparations, Armstrong and coworkers characterized a wide  
54 variety of bonded brush-type CSPs prepared on 2.7  $\mu\text{m}$  SPPs, including cyclofructan-6

55 based,  $\beta$ -cyclodextrin and macrocyclic antibiotics (in particular, teicoplanin, teicoplanin  
56 aglycone and vancomycin) [20]. They first recognized that enantioresolution per analy-  
57 sis time significantly increases going from FPPs to SPPs [13,14], with obvious benefits for  
58 high-throughput screening of chiral compounds. The concept that emerges from these  
59 studies is that chiral SPPs outperform their FPP counterparts in any chromatographic  
60 mode, namely, reversed-phase (RP), normal phase (NP), polar organic and HILIC.

61 In the first part of this paper, we report about the synthesis of novel Pirkle-type Whelk-  
62 O1 2.6  $\mu\text{m}$  chiral SPPs and the kinetic characterization of columns packed with these par-  
63 ticles. To this scope, a comparison between the performance of these columns and those of  
64 columns packed with both 2.5 and 1.8  $\mu\text{m}$  FPPs functionalized with identical chiral selec-  
65 tor [23, 24] was performed by using *trans*-stilbene oxide (TSO) enantiomers as probes. In  
66 the second part of the work, the potential of Whelk-O1 CSPs for ultrafast enantiosepara-  
67 tions on the second/sub-second time-scale is investigated by means of short columns (10  
68 mm packed with both FPPs and SPPs) operated at very high flow rates (up to 8 ml/min).

## 69 2. Experimental section

70 *Columns and materials.* All solvents and reagents employed in this work were purchased  
71 from Sigma-Aldrich (St. Louis, MI, USA). Kromasil silica (1.8 and 2.5  $\mu\text{m}$  particle size,  
72 100 Å pore size, 323 m<sup>2</sup>/g specific surface area) was from Akzo-Nobel (Bohus, Sweden).  
73 Whelk-O1 selector was generously donated by Regis Technologies Inc (Morton Grove,  
74 IL, USA). Accucore silica (2.6  $\mu\text{m}$  particle size, 80 Å pore size, 130 m<sup>2</sup>/g specific surface  
75 area, 0.5  $\mu\text{m}$  shell thickness) was from Thermo Fisher Scientific (Waltham, MA, USA).  
76 150 and 100 mm $\times$ 4.6 mm empty stainless steel columns were from IsoBar Systems by  
77 IDEX (Erlangen, Germany), while 10 $\times$ 4.6 and 10 $\times$ 3.0 mm ones (including their holders)  
78 were fully developed and produced in-house. Fourteen polystyrene standards (from Su-  
79 pelco/Sigma-Aldrich, Milan, Italy) with molecular weights 500, 2000, 2500, 5000, 9000,  
80 17500, 30000, 50000, 156000, 330000, 565000, 1030000, 1570000, 2310000 were employed  
81 for inverse size exclusion chromatography (ISEC).

82 *Equipment.* Two chromatographic equipments were employed in this work. Unless differ-  
83 **ently specified**, the UHPLC chromatographic system used for 150 and 100 mm columns  
84 was an UltiMate 3000 RS system from Thermo Fisher Dionex (**Whaltam, MA, USA**) con-  
85 sisting of a dual gradient RS pump (flow rates up to 8.0 mL/min; pressure limit 800 bar  
86 under NP conditions), an in-line split loop Well Plate Sampler, a thermostated RS Column  
87 Ventilated Compartment and a diode array detector (UV Vanquish) with a low dispersion  
88 2.5  $\mu\text{L}$  flow cell. Detection wavelength was 214 nm (constant filter time: 0.002 s; data col-  
89 lection rate: 100 Hz; response time: 0.04 s). To reduce the extra-column contributions two  
90 350 $\times$ 0.10 mm I.D. Viper capillaries were used to connect the injector to the column and  
91 the column to the detector. The extra-column peak variance (calculated through peak  
92 moments) was 5.5  $\mu\text{L}^2$  in Hex/EtOH 90:10 + 1% MeOH at a flow-rate of 1.0 mL/min  
93 (extra-column volume: 12.2  $\mu\text{L}$ ). Data acquisition, data handling and instrument control  
94 were performed by Chromeleon (vers. 6.8) software.

95 An UPLC Acquity Waters system (**Milford, MA, USA**), equipped with a binary solvent  
96 manager (2mL/min maximum flow rate; pressure limit 1000 bar), an auto-sampler with a  
97 5  $\mu\text{L}$  injection loop, a thermostated column compartment (operated in still air conditions  
98 [5]), a diode array detector with a 500 nL flow cell, 80 Hz acquisition rate (resolution 4.8  
99 nm; no filter time constant) was employed. Two Viper capillaries (250 $\times$ 0.100 mm and  
100 350 $\times$ 0.100 mm  $L\times$ I.D.) were used as inlet and outlet connectors. The extra-column peak  
101 variance (through peak moments) was only 0.91  $\mu\text{L}^2$  at 1.0 mL/min. An updated version  
102 of Empower software was used in order to measure the second central time moments  
103 of the recorded concentration profiles. For the 10 mm columns, a modified version of  
104 the UPLC was used (Fig. S1 of Supplementary Data shows some images of the exper-  
105 imental arrangement). The programmable auto-sampler was replaced with an external  
106 in-house modified sample injector from VICI, **Houston, TX, USA** (model C74U). Essen-  
107 tially, this modification allowed for an electronic and fine control of the switching time  
108 (1.10 s) from injection to loading position and back. The injector is equipped with a 50  
109 nL internal injection loop and a micro-electric actuator (Valco instruments, Houston, TX,

110 USA). The sample solution was introduced through a 25  $\mu\text{L}$  syringe. This arrangement  
111 ensured consistent reduction of tailing effect and high reproducibility between injections.  
112 The standard inlet and outlet connecting tubes were replaced by two PEEK tubings of, re-  
113 spectively, 50 and 60 mm length  $\times$  63.5  $\mu\text{m}$  I.D. With this configuration, the extra-column  
114 peak variance (through peak moments) was only 0.14  $\mu\text{L}^2$  at 1.0 mL/min.

115 *Synthesis of Whelk-O1 SPPs and preparation of columns.* Whelk-O1 SPPs were synthesized  
116 according to the procedure described by Pirkle **and co-workers** in 1992 [25, 26], which has  
117 been also employed for the synthesis of Whelk-O1 FPPs [27–29].

118 CHN elemental analysis for the different silica types functionalized in this work re-  
119 turned the following values: 6.28% C, 0.84% H and 0.73% N for 2.6  $\mu\text{m}$  SPPs; 13.41% C,  
120 1.73% H and 1.39% N for 1.8  $\mu\text{m}$  FPPs; 13.30% C, 1.73% H and 1.38% N for 2.5  $\mu\text{m}$  FPPs.  
121 Calculated bonding densities (based on N) are reported in Table 1. **Details on how these**  
122 **calculations were performed can be found in reference** [30]. FT-IR (KBr) of Whelk-O1  
123 were: 2924, 2864, 1675, 1627, 1548, 1513, 1344, 1078  $\text{cm}^{-1}$ .

124 All columns were slurry packed with a pneumatically driven Haskel pump ( $P_{max} =$   
125 1000 bar). **The slurry solution (10% w/v of Whelk-O1 particles in acetone) was pushed**  
126 **into the column by using a mixture of hexane/2-propanol 90:10 (% v/v) as pushing sol-**  
127 **vent. The pressure was increased from 400 bar up to 1000 bar. 100 mL of pushing solvent**  
128 **were pumped into the column at 1000 bar to consolidate the bed. Decompression until**  
129 **atmospheric pressure was gradually performed.**

130 *van Deemter curve measurements.* The kinetic performance of Whelk-O1 columns was eval-  
131 uated in NP conditions. The mobile phase was a mixture of hexane/ethanol 90:10 (% v/v)  
132 + 1% methanol. Injection volumes were 0.1-0.5  $\mu\text{L}$ . Temperature was set at 35°C. Reten-  
133 tion time ( $t_R$ ) and column efficiency (number of theoretical plates,  $N$ ) of eluted peaks  
134 were automatically processed by the Chromeleon and Empower 3 software (using peak  
135 width at half height, according to European Pharmacopeia).  $N$  values were not corrected  
136 by extra-column contribution. The flow rates employed for studying the dependence of  
137 height equivalent to a theoretical plate  $H (=L/N$ , being  $L$  the column length) on the mo-



138 bile phase velocity started from 0.1 mL/min up to maximum respectively of 4.0 mL/min  
139 (for 100 and 150 mm long columns; equipment: Dionex 3000RS) and 2.0 ml/min (for  
140 10 mm long columns; equipment: Waters Acquity), with constant steps of 0.1 mL/min.  
141 van Deemter curves were plotted as  $H$  vs. interstitial velocity,  $u_{int}$ .  $u_{int}$  was calculated  
142 according to the well known equation:

$$143 \quad u_{int} = \frac{F_v}{\pi r^2 \epsilon_e} \quad (1)$$

144 being  $F_v$  the flow rate,  $r$  the radius of the column and  $\epsilon_e$  the interstitial porosity.  $\epsilon_e$  was  
145 calculated by ISEC experiments, as described below.

146 *ISEC measurements, estimation of interstitial and total porosity and retention factor evaluation.*

147 ISEC measurements were performed by using tetrahydrofuran as mobile phase [31]. In-  
148 jection volume, flow rate and detection wavelength were, respectively, 2  $\mu$ L, 0.1 mL/min  
149 and 254 nm. For ISEC plots, retention volumes were corrected for the extra-column con-  
150 tribution before being plotted against the cubic root of the molecular weight ( $M_W$ ). The  
151 interstitial volume,  $V_e$ , was derived from the extrapolation to  $M_W = 0$  of the linear regres-  
152 sion calculated for the volumes of the totally excluded polystyrene samples [32]. From  
153 this, the estimation of external column porosity,  $\epsilon_e$ , is straightforward (being  $\epsilon_e = V_e/V_{col}$ ,  
154 with  $V_{col}$  the geometric volume of the column). The ISEC estimation of the thermody-  
155 namic void volume,  $V_0$ , was based on the retention volume of benzene. Through this, the  
156 total porosity  $\epsilon_t$  can be calculated ( $\epsilon_t = V_0/V_{col}$ ).

157 The retention factor for the  $i$ -th enantiomer,  $k_i$ , was calculated by:

$$158 \quad k_i = \frac{t_{R,i} - t_0}{t_0} \quad (2)$$

159 where  $t_{R,i}$  is the retention time of the  $i$ -th enantiomer ( $i = 1, 2$ ) and  $t_0$  the void time  
160 calculated by using carbon tetrachloride ( $\text{CCl}_4$ ) as marker.

161 *Specific permeability and Kozeny-Carman constant.* The specific permeability of each column  
162 was calculated according to the traditional equation [33, 34]:

$$k_0 = \frac{u\eta L}{\Delta P} \quad (3)$$

163 where  $u = F_v/\pi r^2$  is the superficial velocity and  $\eta$  the viscosity of the eluent (0.46 cP  
164 for THF at 25°C [35]).  $\Delta P$  is the difference between the total pressure drop,  $P_{tot}$ , and  
165 the system pressure drop (without the column),  $P_{ex}$ .  $P_{ex}$  was measured by replacing the  
166 column with a zero-volume connector. Experimentally,  $k_0$  can be estimated by the slope  
167 of  $\Delta P$  vs.  $u$  plot [36].

168 The Kozeny-Carman constant  $K_c$  was estimated by [33]:

$$K_c = \frac{\epsilon_e^3}{(1 - \epsilon_e)^2} \frac{d_p^2}{k_0} \quad (4)$$

169 where  $d_p$  is the particle size (nominal  $d_p$ s given by manufacturer were used in this work  
170 in place of the more correct Sauter diameter value [5]).

### 171 3. Results and discussion

172 The preparation of SPPs was performed by following the same experimental protocol  
173 described in [27–29] for the functionalization of sub-2 $\mu$ m FPPs. The synthesis is partic-  
174 ularly advantageous and reproducible even on SPPs, since phenomena such as particle  
175 aggregation and clogging or the non-uniform/excessive selector coating, frequently en-  
176 countered with other chiral selectors, do not represent an issue with Whelk-O1 selector.  
177 Table 1 lists the characteristics of the particles employed in this work in terms of dimen-  
178 sion, specific surface area, pore size (data from manufacturers) and chiral-selector loading  
179 (see Experimental section). Surface coverage is given both as  $\mu$ mol per gram of bare sil-  
180 ica (column 6 of Table 1) and  $\mu$ mol per square meter (column 7). Several things can be  
181 observed from this table. The first is that the synthesis of FPPs of different dimensions is  
182 extremely reproducible (practically the same loading of chiral selector, about 390  $\mu$ mol/g  
183 or 1.2  $\mu$ mol/m<sup>2</sup>, was found on the 1.8 and 2.5  $\mu$ m FPPs). The second is that, by keeping  
184 constant the experimental conditions, functionalization of bare silica leads to significantly  
185 larger surface coverage of chiral selector (+ 20%) on SPPs (1.5  $\mu$ mol/m<sup>2</sup>) than on fully  
186 porous ones (1.2  $\mu$ mol/m<sup>2</sup>). **This could be due to different reasons such as larger acces-**  
187 **sibility of external layers of particles, different surface chemistry of base silica FPPs and**

188 SPPs, etc. However, it is difficult to generalize these findings. They are indeed consistent  
189 with previous reports by Armstrong and coworkers [20, 21], but contrast with other data  
190 from the same group [37]. even though it is still uncertain why this happens (larger acces-  
191 sibility of external layers of particles, different surface chemistry of FPPs and SPPs, etc.).  
192 Obviously, since the specific area per gram of FPPs is larger than that of SPPs, the total  
193 amount of chiral selector bounded per gram of base silica is also greater on the former  
194 type of particles than on fused-core ones. This finding is consistent with previous reports  
195 by Armstrong and coworkers [13,14], even though it is still uncertain why this happens  
196 (larger accessibility of external layers of particles, different surface chemistry of FPPs and  
197 SPPs, etc.).

198 The common understanding is that the larger the amount of chiral-selector tethered  
199 to the surface, the larger the loadability of the phase (which is definitely important in  
200 preparative applications [38–40]) and the larger the retention factor. On the other hand,  
201 the relationship between enantioselectivity and surface coverage of chiral selector is not  
202 straightforward, since this last could impact also on the adsorption-desorption kinetics  
203 and thus on the separation efficiency. relationship between The resolution,  $R_s$ , of two  
204 chromatographic peaks (defined by the peak separation divided by the mean peak width)  
205 can be indeed expressed as [41]:

$$206 \quad R_s = \frac{\sqrt{N} \alpha - 1}{2} \frac{\bar{k}}{\alpha + 1} \frac{1}{1 + \bar{k}} \quad (5)$$

207 where  $N$  is the number of theoretical plates, and  $\bar{k}$  and  $\alpha$  are, respectively, the average  
208 retention factor (i.e., the average of retention factors of the two enantiomers) and the  
209 selectivity, defined by [42]:

$$210 \quad \alpha = \frac{k_2}{k_1} \quad (6)$$

211 According to Eq. 5, one observes that resolution not only depends on the fact that solutes  
212 must be retained ( $\bar{k} \neq 0$ ) and that they must be retained at different extent ( $\alpha \neq 1$ ), but also  
213 on the efficiency of the column, the larger being the efficiency, the higher the resolution  
214 with higher efficiencies giving better resolution.

215 Fig. 1 shows the chromatograms recorded for the separation of TSO enantiomers on,  
216 respectively, the 150×4.6 mm I.D. column packed with 2.5 μm FPPs (top), the 100×4.6  
217 mm I.D. one packed with 1.8 μm FPPs (middle) and, finally, the 150×4.6 mm I.D. column  
218 packed with 2.6 μm SPPs (bottom). On each column, the flow rate (see figure caption)  
219 at which the chromatogram was recorded corresponds to the optimal flow rate, that is  
220 where the van Deemter curve presents its minimum (see later on). For the sake of com-  
221 parison between different columns, the x-axis is expressed as retention factor (in place  
222 of the traditional retention time). Retention factors were calculated by using CCl<sub>4</sub> as the  
223 void volume marker (see the experimental section). As it can be noticed from Fig. 1, on  
224 the two columns packed with 2.5 μm and 1.8 μm FPPs, TSO enantiomers are character-  
225 ized by the same retention factors ( $k_1 = 0.69$  and  $k_2 = 1.72$ ), with  $\alpha$  equal to 2.49. On  
226 the other hand, on the column packed with 2.6 μm SPPs, retention of both enantiomers  
227 is smaller ( $k_1 = 0.50$  and  $k_2 = 1.27$ ) but  $\alpha$  is slightly larger (2.54). On the same figure  
228 the efficiency ( $N/m$ ) of each peak has also been reported.  $N$  was calculated as described  
229 in the experimental section. In all cases, very large values were observed. In particular,  
230 on the 100×4.6 mm I.D. column packed with 1.8 μm FPPs (middle chromatogram), an  
231 efficiency as large as 292,000 and 271,000  $N/m$  was obtained respectively for the first and  
232 the second eluted enantiomer. As a marginal remark, **we it can be observed** that these  
233 values are typical of efficient RP systems [5, 36]. The resolution of columns, estimated  
234 by eq. 5, resulted very large as well.  $R_s$  is 19.6 on the column packed with 1.8 μm FPPs,  
235 20.2 for the column packed with 2.5 μm FPPs and 17.3 on the column packed with core-  
236 shell particles. Therefore, **in spite of the highest density of chiral-selector (see Table 1), the**  
237 **column packed with SPPs has the lowest  $R_s$ , even if the surface density of chiral-selector**  
238 **measured on these particles was the highest (Table 1). However, the overall much higher**  
239 **surface area for FPPs can outweigh this feature and explain this fact.** The difference in  $R_s$   
240 between columns packed with FPPs **simply reflects could reflect not only** the difference in  
241 column length and thus in the total  $N$  per column (Fig. S2 of Supplementary Data graph-  
242 ically shows this concept by reporting, for the three columns,  $N$  per column as a function

243 of velocity) **but also the impact of particle size (1.8 vs. 2.5  $\mu\text{m}$ ) on the measured efficiency.**  
244 On the other hand, to explain the smallest  $R_s$  measured on the core-shell column one has  
245 to consider that the very favourable contribution of  $\alpha$  is ruled out by both the effect of  
246 efficiency and retention.

247 Table 2 reports some of the physico-chemical parameters in use to assess the quality  
248 of column packing, at least from a qualitative viewpoint, such as the external porosity,  $\epsilon_e$ ,  
249 and the Kozeny-Carman constant (see Eq. 4). For well packed columns,  $\epsilon_e$  is roughly 0.4  
250 [1, 43] and 0.37 [5, 44] respectively for beds made of core-shell and fully porous particles  
251 and the  $K_c$  constant is close to 180 [33]. As it can be seen from this table, for all columns  
252  $\epsilon_e$  was about 40%. However, while the columns packed with FPPs have  $K_c$  equal to 180,  
253 for the one packed with SPPs  $K_c$  is only 160. For the sake of completeness, in Table 2, the  
254 total porosities,  $\epsilon_t$ , of columns are also reported (see the experimental section for details).  
255 Their values are close to typical values for columns packed with fully porous (0.65-0.7)  
256 and core-shell (0.52-0.55) particles [32, 39, 45].

257 The other important information that can be derived from Table 2 is about the per-  
258 meability (see Eq. 3) of columns. As expected, the column packed with 1.8  $\mu\text{m}$  FPPs is  
259 characterized by the smallest  $k_0$  value,  $2.95 \times 10^{-11} \text{ cm}^2$ , which reflects the difficulty of  
260 delivering a flow in a bed made of very fine particles. Surprisingly, the column packed  
261 with 2.6 SPPs results to be about 25% more permeable than that packed with 2.5 FPPs,  
262 even though their  $\epsilon_e$  are very similar. ~~Together with the already discussed low value of  $K_c$ ,~~  
263 ~~this could suggest a less efficient packing of SPPs (see later on).~~ **This could suggest a less**  
264 **dense packing of SPPs that, together with the already discussed low value of  $K_c$ , could**  
265 **affect the kinetic performance of the column.**

266 When the van Deemter equation is employed in chiral chromatography, in addition  
267 to the traditional terms describing longitudinal diffusion ( $B$ ), eddy dispersion ( $A$ ) and  
268 solid-liquid mass transfer kinetics ( $C_s$ ), an additional term taking into account the slow  
269 adsorption-desorption kinetics ( $C_{ads}$ ), which frequently characterizes enantio-recognition  
270 phenomena, is also added [4, 46]. The dependence of  $H$  on the mobile phase velocity is

271 therefore written as:

$$272 \quad H = A(u) + \frac{B}{u} + C_S u + C_{ads} u \quad (7)$$

273 Fig. 2 shows the van Deemter curves of TSO enantiomers measured, respectively, on the  
274  $150 \times 4.6$  mm column packed with  $2.5 \mu\text{m}$  FPPs (top), on the  $150 \times 4.6$  mm one packed with  
275  $2.6 \mu\text{m}$  SPPs (middle) and on the  $100 \times 4.6$  mm column packed with  $1.8 \mu\text{m}$  FPPs (bottom).  
276 Diamonds (green) refer to the first enantiomer and circles (blue) to the second one. The  
277 height equivalent to a theoretical plate has been plotted against the interstitial velocity,  
278  $u_{int}$  (Eq. 1), which represents the true linear velocity of the mobile phase (since the fluid  
279 flows around and between the particles, not through them). These plots suggest some  
280 considerations. First, one may observe that the longitudinal diffusion of the two enan-  
281 tiomers in each column is the same. This is demonstrated by the overlapping of their  
282 van Deemter curves at low flow rates (where the  $B$ -term is dominant). Then, under the  
283 assumption of the same eddy dispersion for the two enantiomers in a given column [47],  
284 the conclusion is reached that the difference in the van Deemter curves (already evident at  
285 relatively low linear velocity, starting at  $u_{int}$  roughly  $0.3$  cm/s) is essentially due to a slow  
286 adsorption-desorption process. This is particularly evident for the column packed with  
287  $2.6 \mu\text{m}$  SPPs (middle plot). Another interesting observation coming from Fig. 2 is that the  
288 slope of the  $C$ -branch of the van Deemter equation is markedly steeper for the column  
289 packed with  $1.8 \mu\text{m}$  FPPs (bottom part of the figure) than for columns packed with both  
290  $2.5 \mu\text{m}$  FPPs (top) and  $2.6 \mu\text{m}$  SPPs (middle). This is due to frictional heating generated by  
291 the stream of mobile phase against the packed bed of the column through which it perco-  
292 lates under significant pressure gradient [48–50]. For instance, at  $u_{int}=0.8$  cm/s, the back-  
293 pressure generated by the  $1.8 \mu\text{m}$  column was 5300 psi and, at  $u_{int}=1.0$  cm/s, it reached  
294 6750 psi. The heat produced locally is dissipated in both the radial and longitudinal direc-  
295 tion of the column. This generates longitudinal and radial temperature gradients, whose  
296 amplitude depends on the degree of thermal insulation of the column (either adiabatic  
297 or isothermal). The column compartment of the Dionex UHPLC equipment used for the  
298 measurement of the van Deemter curves with these columns (see Experimental section)

299 can only work in the so-called forced-air mode (quasi-isothermal conditions), where it is  
300 well known that radial temperature gradients degrade the efficiency of column [51–53].

301 With the purpose of comparing the behavior of the three columns, in Fig. 3 van  
302 Deemter curves of the first and the second TSO enantiomer are overlapped. Curves on  
303 top of this figure are those for the less retained enantiomer, while on the bottom there are  
304 the van Deemter curves relative to the second enantiomer. The kinetic behavior of the  
305 first enantiomer looks very similar on all columns, in consequence of the very low reten-  
306 tion (see Fig. 1) of this compound that does not allow to draw any significant conclusion  
307 on mass transfer phenomena. The only minor difference is around the minimum of van  
308 Deemter curves, where the core-shell column is the less efficient (see later on).

309 By considering the second enantiomer (bottom part of Fig. 3), very different kinetic  
310 behaviors can be observed, depending on column. Unexpectedly, the column packed  
311 with Whelk-O1 2.6  $\mu\text{m}$  SPPs (circles, purple), no matter the flow rate, is characterized by  
312 the worst performance, even worse than its 2.5  $\mu\text{m}$  fully porous counterpart (diamonds,  
313 cyan). This is a surprising result that contrasts with the commonly observed performance  
314 of columns packed with  $\text{C}_{18}$  SPPs [6, 7]. It can be explained by considering the con-  
315 tribution to band broadening coming from either eddy dispersion or slow adsorption-  
316 desorption kinetics or a combination of both. The first statement, about the importance  
317 of eddy dispersion in columns packed with SPPs ~~is not supported by literature data, as it~~  
318 ~~was mentioned before~~, **is counter intuitive at least according to literature data that demon-**  
319 **strate how packed beds made of SPPs are expected to be more efficient than those of FPPs**  
320 **(see before)**. It ~~is~~ **can be** however suggested by the experimental difficulties encountered  
321 during the slurry packing of Whelk-O1 SPPs. By considering their characteristics, first of  
322 all that these particles are polar, however it does not seem weird that they behave differ-  
323 ently from hydrophobic  $\text{C}_{18}$  ones during the slurry packing [19, 54]. As a matter of fact,  
324 not only the achievement of stable slurry suspensions was more difficult with very polar  
325 SPPs than with Whelk-O1 fully porous ones but also, e.g., the time needed **to compress**  
326 **the bed (by high-pressure flushing)** ~~for bed consolidation~~ did not follow any expected

327 trend and could not be optimized. Even if, undoubtedly, more investigation is needed in  
328 this field, in particular on the rheological characteristics of Whelk-O1 SPPs, **In conclusion,**  
329 the impression is that one of the most important characteristics of hydrophobic core-shell  
330 particles, i.e. their ability to generate **very efficient** packed beds characterized by very  
331 ~~low eddy dispersion~~, could not be easily reproducible with very polar Whelk-O1 SPPs.  
332 **Further investigation is needed to assess this point, in particular on rheological charac-**  
333 **teristics of Whelk-O1 SPPs.** In agreement with [11, 12], ~~we may~~ **it should be** concluded  
334 ~~this reasoning by saying~~ that the efficient preparation of packed beds of polar SPPs still  
335 requires a long way to go. This essentially needs the optimization of all steps of packing  
336 protocol, without which the full potential of polar chiral SPPs can be barely reached.

337 As mentioned before, on the 2.6  $\mu\text{m}$  Whelk-O1 core-shell column the contribution  
338 to band broadening coming from a slow mass transfer process seems to be particularly  
339 evident. Since the solid-liquid mass transfer term ( $C_s$ ) should be lower on core-shell than  
340 on fully porous particles (due to the presence of the inaccessible core), the conclusion  
341 is that the adsorption-desorption kinetics must be slower on core-shell particles (higher  
342  $C_{ads}$  term in eq. 7) than on the fully porous ones. An explanation could be the different  
343 surface density of chiral selector between core-shell and FPPs. Table 1 shows that this  
344 surface density is about 20% larger on SPPs than on fully porous ones. In literature there  
345 are practically no studies which have attempted to assess if and how chiral recognition is  
346 modified by changing the amount of chiral selector tethered to the surface and how this  
347 could impact on the chromatographic performance [12]. On the other hand, ~~we believe~~  
348 this is a very important subject that needs more experimental and theoretical work to be  
349 fully understood.

350 Finally, by still looking at the bottom part of Fig. 3, it is evident that the column  
351 packed with 1.8  $\mu\text{m}$  FPPs (triangles, green) outperform the other two in terms of kinetic  
352 behavior but it is also clear that, at high flow rates, where the effect of frictional heating  
353 on efficiency is dominant, this column does not offer any advantage over the one packed  
354 with 2.5  $\mu\text{m}$  FPPs. Indeed, at  $u_{int}$  slightly larger than 1 cm/s, the C-branch of the 1.8  $\mu\text{m}$



355 fully porous column merges to that of the column packed with 2.5  $\mu\text{m}$  FPPs.

356 Fig. 4 (top) shows the gain in analysis time that can be obtained by moving from both  
357 the columns packed with 2.5  $\mu\text{m}$  FPPs and 2.6  $\mu\text{m}$  SPPs to that packed with 1.8  $\mu\text{m}$  FPPs.  
358 The necessary premise to discuss this figure – whose meaning, ~~we want to point out,~~ is  
359 merely practical – is that the length of commercially available columns packed with 2.5-  
360 2.7  $\mu\text{m}$  particles (no matter if fully porous or pellicular) is usually 150 mm, while that of  
361 columns packed with sub-2 $\mu\text{m}$  particles is only 100 mm or less. This justifies the direct  
362 comparison presented in Fig. 4, where column length is not accounted for. Having ac-  
363 knowledged this, and by referring for each column to condition of maximum efficiency  
364 (indeed chromatograms presented in Fig. 4 were recorded at the optimum flow rate, see  
365 figure caption for details), one observes that the column packed with 1.8  $\mu\text{m}$  FPPs permits  
366 to ~~gain~~ **decrease analysis time** more than 50 and 30% ~~of analysis time~~ (here simply calcu-  
367 lated as the retention time of the second eluted enantiomer) with respect to, respectively,  
368 the 2.5  $\mu\text{m}$  fully porous column and the 2.6  $\mu\text{m}$  core-shell one. The practical advantage  
369 achievable with the 100 mm column packed with sub-2 $\mu\text{m}$  particles, becomes still more  
370 evident by considering, in addition to analysis time, also the resolution of columns (see  
371 before). Thus, the ratio between resolution and analysis time [55], graphically given as  
372 bar chart in the bottom part of Fig. 4, is strongly favorable for the 1.8  $\mu\text{m}$  column packed  
373 with FPPs (it is indeed 11.9 on this column vs. 5.3 and 7.9 on, respectively, the 2.5  $\mu\text{m}$   
374 fully porous and the 2.6  $\mu\text{m}$  core-shell column). Incidentally, the gain of  $R_s/t_{R,2}$  ratio ob-  
375 served for the 2.6  $\mu\text{m}$  core-shell column over that packed with 2.5  $\mu\text{m}$  FPPs comes from  
376 the reduction of retention time in the former column (due to a much lower total surface  
377 area per column) and not from an increase of  $R_s$  (which actually is larger on the 2.5  $\mu\text{m}$   
378 fully porous column).

379 The last part of this study briefly reports on the use of short columns, packed with both  
380 Whelk-O1 FPPs and SPPs, to realize ultrafast enantioseparations. In this proof-of-concept  
381 study, 10 mm columns of different I.D. (3.0 and 4.6 mm) were employed. These columns  
382 were in-house designed and developed. Fig. S3 of Supplementary Data shows a picture

383 of the 10 mm column and holder. They were packed by following the same protocol also  
384 used for longer columns. Table 3 has some information that helps to characterize these  
385 columns, in particular the optimal flow rate (i.e., the flow rate corresponding to the min-  
386 imum of van Deemter curve), the corresponding interstitial linear velocity and the maxi-  
387 mum efficiency (in  $N/m$ ). With the purpose of performing ultrafast enantioseparations,  
388 these columns were operated at the maximum flow achievable by our instrumentation  
389 (8 ml/min). Accordingly, the Thermo Dionex equipment (see experimental section) was  
390 employed, even though its extra-column variance is not negligible with respect to that of  
391 first and second eluted enantiomers (respectively, roughly 11.2 and 28  $\mu\text{L}^2$ ). In the last  
392 column of Table 3, the number of theoretical plates per column measured at the highest  
393 flow rate is reported. As an example, Fig. 5 shows the chromatogram recorded with the  
394  $10 \times 3.0$  mm column packed with 1.8  $\mu\text{m}$  FPPs. As it can be seen, the separation of TSO  
395 enantiomers was performed in less than 1 s, with  $R_s = 2.2$ . This represents an extraordi-  
396 nary result, unimaginable only a few years ago in chiral liquid chromatography, **which is**  
397 **even comparable with that of chiral separations on microchip platforms [56].**

#### 398 4. Conclusions

399 The investigation of the kinetic performance of columns packed with Whelk-O1 fully  
400 porous and core-shell particles of similar diameter (2.5  $\mu\text{m}$  for FPPs vs. 2.6  $\mu\text{m}$  for core-  
401 shell ones) has surprisingly revealed that FPPs outperform SPPs. This depends, in part,  
402 on the faster mass-transfer adsorption-desorption kinetics observed (especially on the  
403 second eluted enantiomer) on the FPPs and, in part, on the smaller eddy dispersion con-  
404 tribution to band broadening on the column packed with FPPs. The slower mass-transfer  
405 adsorption-desorption process is most likely due to the larger surface density of chiral  
406 selector on the SPPs. Indeed, even though the same experimental conditions were main-  
407 tained during functionalization of SPPs and FPPs, the outcome was different. The surface  
408 density of Whelk-O1 selector on SPPs was **indeed** 20% larger than that of FPPs. ~~This find-~~  
409 ~~ing is consistent with previous results from Armstrong et al. [13,14] and seems to be a~~

410 ~~characteristic feature in the derivatization of core-shell particles. Our~~ **These** results sug-  
411 gest that, at least for the case considered in this work, the higher the surface coverage, the  
412 lower the adsorption-desorption process but with the information in our possession no  
413 generalization can be made. Fundamental studies aimed at investigating the relationship  
414 between mass transfer kinetics and surface density of chiral selector are needed.

415 On the other hand, the empirical difficulty to pack Whelk-O1 core-shell particles ex-  
416 plains the important eddy dispersion contribution to band broadening in columns packed  
417 with these particles. Different attempts have been done to improve the packing process,  
418 by varying many experimental variables (slurry composition, consolidation time, etc.)  
419 during the packing, but without success. These findings show that packing polar SPPs is  
420 significantly different from packing hydrophobic SPPs (such as C<sub>18</sub> particles), for which  
421 a large amount of information and expertise has been collected over the years. One of the  
422 most significant characteristics of beds made of C<sub>18</sub> core-shell particles is their extremely  
423 low eddy dispersion term. This, however, seems to be difficult to achieve with Whelk-O1  
424 SPPs. The investigation of rheological properties of these particles can help to understand  
425 their different behavior with respect to fully porous particles so to optimize the packing  
426 protocol and, thus, the kinetic performance of columns made of polar Whelk-O1 SPPs.

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## 433 **Appendix A. Supplementary Data**

434 Supplementary data associated with this article can be found in the online version.

## 435 6. Figures and Tables

### 436 Figure captions

437 **Fig 1.** Chromatograms showing the separation of TSO enantiomers on the three columns  
438 employed in this work. **Carbon tetrachloride was used as dead time marker.** Top: 150×4.6  
439 mm column packed with Whelk-O1 2.5  $\mu\text{m}$  FPPs; middle: 100×4.6 mm column packed  
440 with Whelk-O1 1.8  $\mu\text{m}$  FPPs; bottom: 150×4.6 mm column packed with Whelk-O1 2.6  
441  $\mu\text{m}$  SPPs. Chromatograms were recorded at the flow rate corresponding to the minimum  
442 of the van Deemter curve (they were, from top to bottom, respectively 1.2, 1.8 and 1.5  
443 ml/min). For the sake of comparison, x-axis is given in terms of retention factor instead  
444 of retention time. Close to each peak, efficiency ( $N/m$ ), retention factor ( $k$ ) and retention  
445 time ( $t_R$ ) are indicated. **Instrument employed for measurements: UPLC Waters Acquity.**

446  
447 **Fig 2.** van Deemter curves for TSO enantiomers measured on Whelk-O1 columns (same  
448 geometries as in Fig. 1) packed with, respectively, 2.5  $\mu\text{m}$  FPPs (top), 2.6  $\mu\text{m}$  SPPs (mid-  
449 dle) and 1.8  $\mu\text{m}$  FPPs (bottom). **Instrument employed for measurements: Dionex 3000RS.**

450  
451 **Fig 3.** Overlapped van Deemter curves measured on the three Whelk-O1 columns (same  
452 geometries as in Fig. 1), respectively for the first (top) and the secondly (bottom) eluted  
453 TSO enantiomers. Diamonds: column packed with 2.5  $\mu\text{m}$  FPPs; circles: column packed  
454 with 2.6  $\mu\text{m}$  SPPs; triangles: column packed with 1.8  $\mu\text{m}$  FPPs. **Instrument employed for**  
455 **measurements: Dionex 3000RS.** See text for details.

456  
457 **Fig 4.** A) Same chromatograms as in Fig. 1, **showing the separation of TSO enantiomers**  
458 **on the three columns employed in this work,** but with the x-axis given in retention time.  
459 **Carbon tetrachloride was used as dead time marker.** B) Bar chart showing the ratio be-  
460 tween resolution and retention time for the 2.6  $\mu\text{m}$  core-shell column (first bar on the left,  
461 blue color), the 1.8  $\mu\text{m}$  fully porous column (middle bar, orange) and, finally, the 2.5  $\mu\text{m}$

462 fully porous column (last bar on the right, red). Ratios were calculated on the second  
463 eluted enantiomer. **Instrument employed for measurements: UPLC Waters Acquity.**

464

465 **Fig 5.** Example of ultrafast enantioseparation thanks to the use of short column and high  
466 flow rate. In this particular case, a 10×3.0 mm column packed with 1.8 μm FPPs was  
467 operated at 8 ml/min ( $u_{int} = 4.8$  cm/s) **for the separation of TSO enantiomers. Carbon**  
468 **tetrachloride was used as dead time marker.** Note the time scale in seconds. **Instrument**  
469 **employed for measurements: Dionex 3000RS.** See text for details.

470

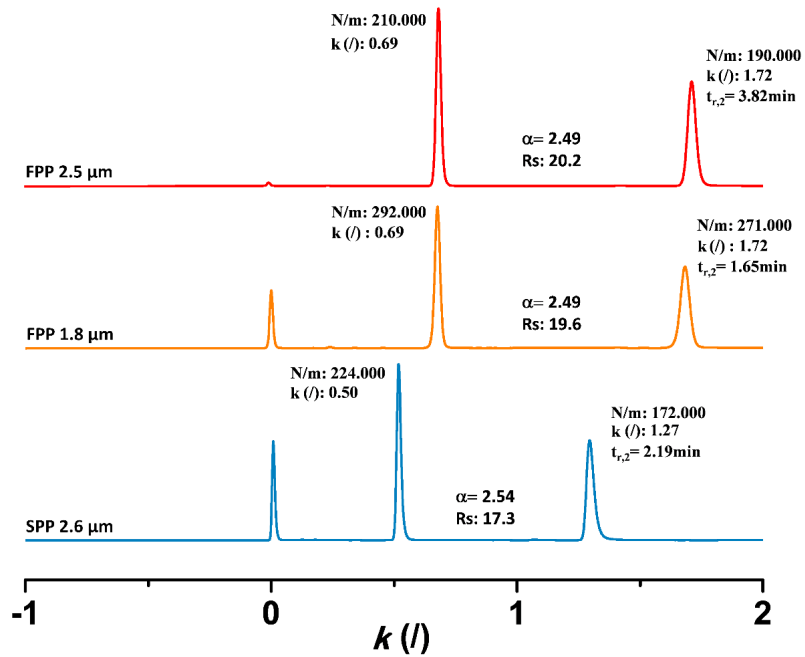


Figure 1:

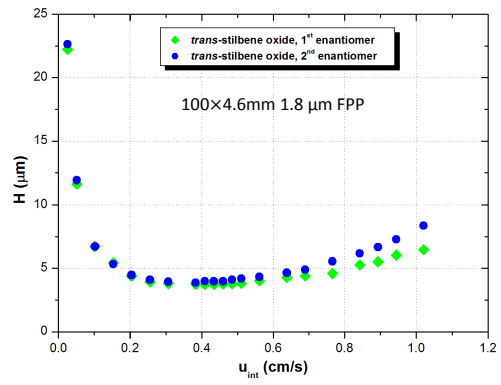
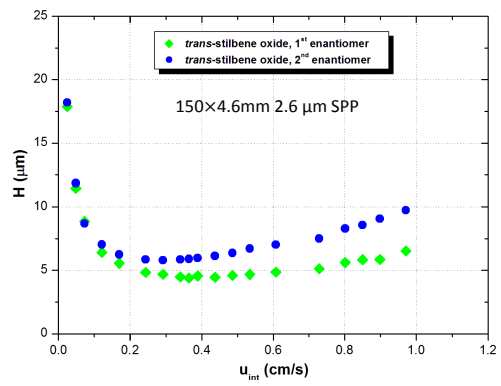
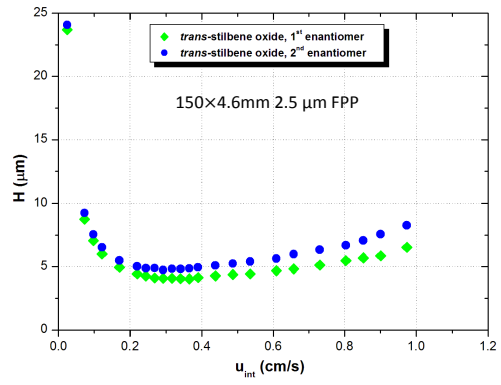


Figure 2:

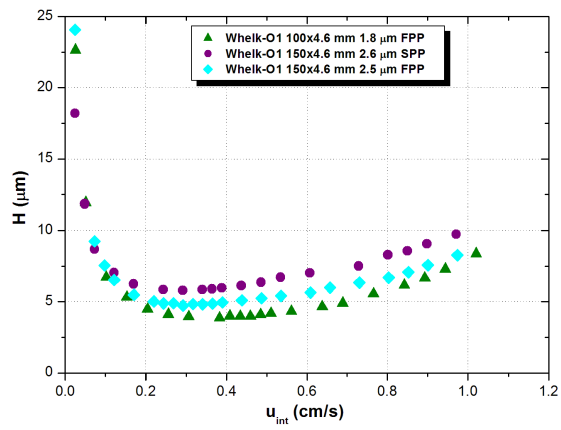
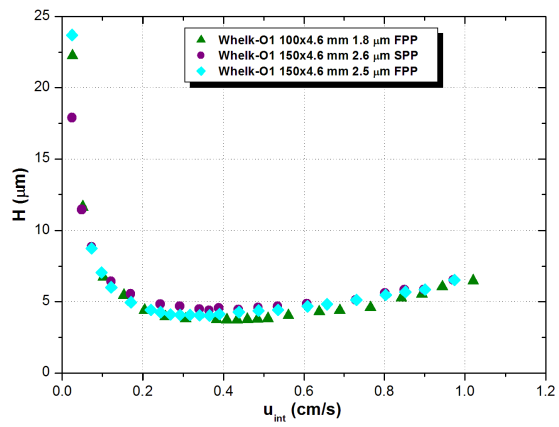


Figure 3:



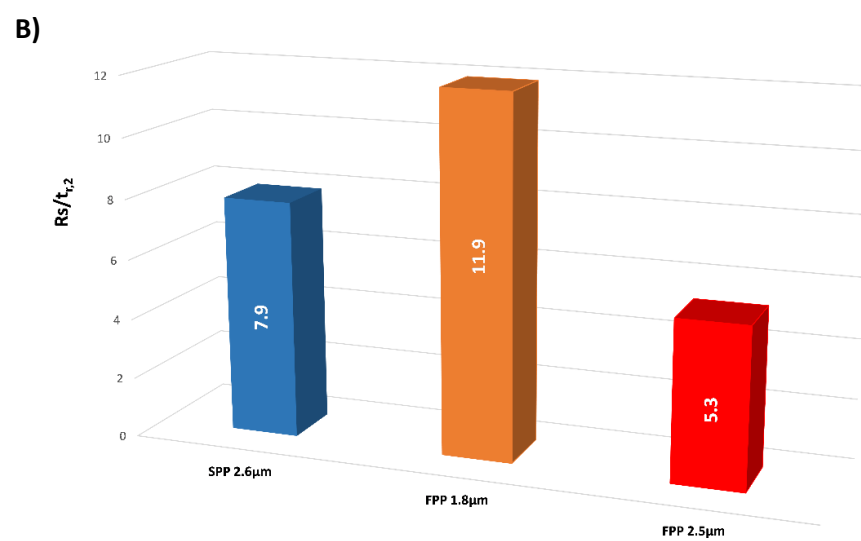
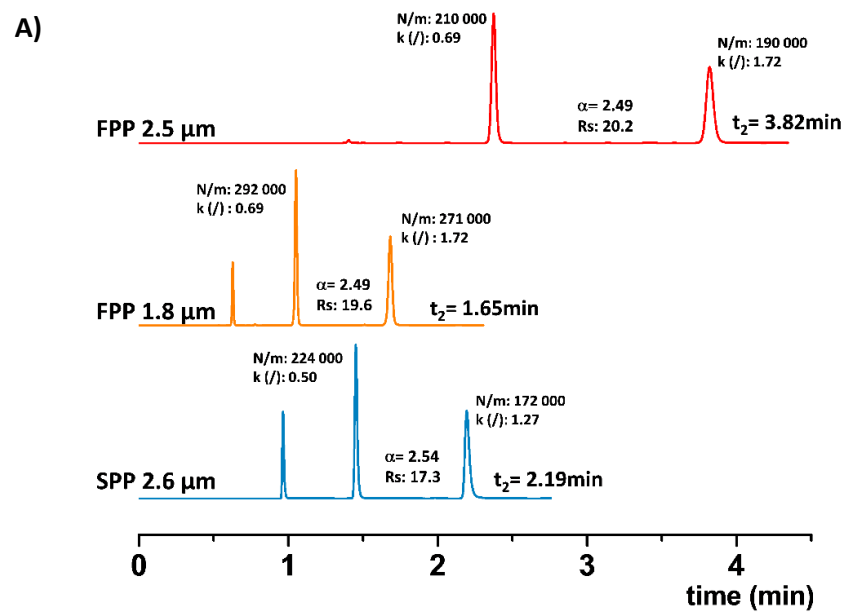


Figure 4:

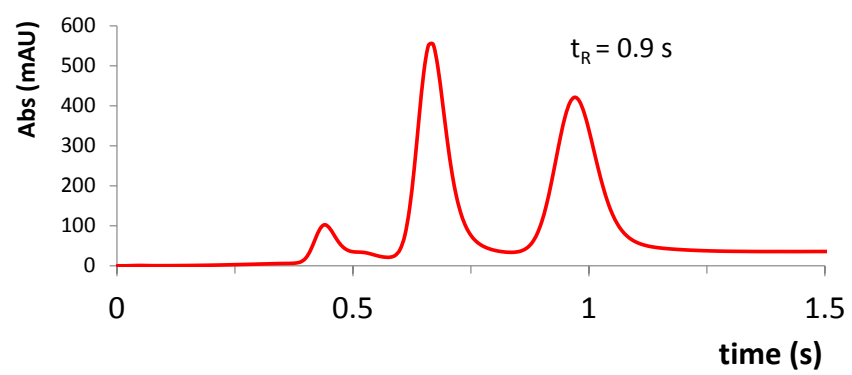


Figure 5:

Table 1: Geometrical characteristics of Whelk-O1 columns: particle type (FP: fully porous, SP: superficially porous); column dimensions; particle diameter ( $d_p$ ); specific surface area ( $A_s$ ); pore size; bonding density (given both as  $\mu\text{mol}$  per gram of bare silica and  $\mu\text{mol}$  per square meter).

Particle type	Dimensions (L×I.D., mm)	$d_p$ ( $\mu\text{m}$ )	$A_s$ ( $\text{m}^2/\text{g}$ )	Pore size ( $\text{Å}$ )	Bonding density ( $\mu\text{mol}/\text{g}$ ) ( $\mu\text{mol}/\text{m}^2$ )	
FP	150×4.6	2.5	323	100	391.2	1.21
FP	100×4.6	1.8	323	100	394.6	1.22
SP	150×4.6	2.6	130	80	189.8	1.46

Table 2: Physico-chemical properties of Whelk-O1 columns: particle type (FP: fully porous, SP: superficially porous); total porosity ( $\epsilon_t$ ); external porosity ( $\epsilon_e$ ); Kozeny-Carman constant ( $K_c$ ); permeability ( $k_0$ ).

Particle type	$\epsilon_t$	$\epsilon_e$	$K_c$	$k_0 \times 10^{11}$ (cm <sup>2</sup> )
FP	0.670	0.412	180	7.06
FP	0.644	0.393	180	2.95
SP	0.524	0.413	160	8.60

Table 3: Kinetic performance (in  $N/m$ ) of short columns (10 mm) of different diameter.  $F_{v,opt}$  and  $u_{int,opt}$  represent, respectively, the optimum flow rate (that is the flow rate corresponding to the minimum of the van Deemter curve) and the optimum interstitial velocity;  $N_{max}$  is the number of theoretical plates per column, when the column was operated at 8 ml/min (see text for more details). In all cases,  $N$  has been calculated as the average value of  $N_s$  of the two TSO enantiomers. Particle type: FP, fully porous; SP, superficially porous). **Instruments employed for measurements: UPLC Waters Acquity for van Deemter curves; Dionex 3000RS for ultrafast enantioseparations (evaluation of  $N_{max}$ ).**

Particle type	L×I.D. (mm)	$F_{v,opt}$ (mL/min)	$u_{int,opt}$ (cm/s)	$N/m$	$N_{max}$
FP	10×4.6	1.7	0.43	190,000	1220
SP	10×4.6	1.5	0.36	140,000	850
FP	10×3.0	0.7	0.42	180,000	520

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## \*Highlights (for review)

- 1) Novel Pirkle-type Whelk-O1 core-shell chiral stationary phase was prepared
- 2) Difficulty of efficiently packing polar core-shell particles is reported
- 3) Effect of surface coverage on adsorption-desorption kinetics is pointed out
- 4) Kinetic characterization of new stationary phase in normal phase mode is described
- 5) Separation of enantiomers in less than 1 second was achieved

# Pirkle-type chiral stationary phase on core-shell and fully porous particles: are superficially porous particles always the better choice towards ultrafast high-performance enantioseparations?

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## Abstract

Pirkle-type Whelk-O1 chiral stationary phase (CSP) was prepared on 2.6  $\mu\text{m}$  superficially porous particles (SPPs). The chromatographic behavior of columns packed with this new CSP was compared with that of columns packed respectively with 1.8 and 2.5  $\mu\text{m}$  Whelk-O1 fully porous particles (FPPs). In the comparison, both thermodynamic and kinetic aspects were considered. Contrary to initial expectations, chiral columns packed with 2.6  $\mu\text{m}$  SPPs were quasi-comparable to those packed with 2.5  $\mu\text{m}$  FPPs, apparently due to larger contributions to band broadening from both eddy dispersion and, especially for the second eluted enantiomer, adsorption-desorption kinetics. These findings raise the question if SPPs, in spite of the undeniable advantages of their morphology to speed up mass transfer, are always the best choice for high-efficient ultrafast chiral separations. The last part of the work focuses on the use of short columns (10 mm long) and very high flow rates to realize the separation of the enantiomers of *trans*-stilbene oxide (TSO) in normal phase mode in less than one second.

**Keywords:** Whelk-O1 superficially porous chiral stationary phase; ultrafast

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## 1. Introduction

Last generation superficially-porous particles (SPPs) [1, 2], referred to also as core-shell, fused-core or solid-core particles, are made of a non-porous fused silica core surrounded by a porous shell, whose volume is usually 60-75% of particle volume. In terms of mass transfer, core-shell structure offers some advantages over that of a fully porous particle (FPP) since the contributions to band broadening from both the longitudinal diffusion due to the relaxation of axial gradient concentration along the column (the so called *B*-term of the van Deemter equation) and the solid-liquid mass transfer resistance due to the diffusion across the particle (*C*-term of the van Deemter equation) are reduced by the presence of the inaccessible core. In addition, columns packed with  $C_{18}$ -SPPs have been demonstrated to be extremely efficient also thanks to the very low eddy diffusion, which comes from flow unevenness in the interstitial zone of the column (*A*-term of the van Deemter equation) [3–5]. Even though the explanation of the low *A*-term for columns packed with  $C_{18}$  SPPs remains to a large extent unknown, the most accepted hypothesis is that roughness of core-shell particles limits particle slipping after releasing the high pressure employed for the preparation of the packed bed by slurry-packing, therefore reducing radial bed heterogeneity [1, 2]. The reason of the great success of SPPs is that they have provided a reasonable compromise between two opposite tendencies. Indeed, the tendency to improve analytical throughputs by means of columns packed with smaller and smaller particles and reduced dimensions is limited by instrumental factors, such as the extremely high pressures needed to operate these columns at high flow rates, on the one hand, and the effect of system extra-column volume on peak broadening, on the other. As a matter of fact, columns packed with  $2.7\ \mu\text{m}$  SPPs are able to provide essentially the same efficiency as columns packed with sub  $2\text{-}\mu\text{m}$  FPPs (keeping constant column dimensions and experimental conditions), but at operating pressures similar to those of columns packed with  $3\ \mu\text{m}$  FPPs [6, 7].



27 Surprisingly, the employment of SPPs in chiral chromatography is relatively recent  
28 [8]. The first work describing the use of SPPs in chiral HPLC dates 2011, when Lind-  
29 ner and coworkers prepared [9] a cinchona alkaloid based anion exchanger CSP by using  
30 2.7  $\mu\text{m}$  fused-core particles as base material. The column was successfully employed for  
31 the enantioseparation of amide type amino acid derivatives, even if the authors do not  
32 mention the possible advantages given by this typology of CSP. Chankvetadze and al.  
33 [10] firstly compared the kinetic performance of CSPs prepared on polysaccharide-coated  
34 FPPs and SPPs. They mentioned some of the benefits of chiral SPPs over their fully porous  
35 counterparts, such as an higher enantioselectivity at comparable content of chiral selec-  
36 tor, a limited dependence of plate height on mobile phase flow rate and a larger enan-  
37 tioreolution per analysis time, with obvious benefits for high-throughput screening of  
38 chiral compounds [10]. By using 4.6 mm I.D.  $\times$  250 mm columns, they demonstrated that  
39 columns packed with SPPs outperform those packed with FPPs in terms of efficiency and  
40 speed of analysis. Fanali and coworkers [11, 12] employed the same polysaccharide-based  
41 chiral particles used in [10] to pack capillary columns (75  $\mu\text{m}$  I.D.  $\times$  25 cm) for nano-liquid  
42 chromatography and electrochromatography experiments. They report about the diffi-  
43 culty to efficiently operate these capillaries. They conclude that, without further optimiza-  
44 tion, this column format does not allow to reach useful efficiency for high-performance  
45 separation. Even if the authors do not discuss in detail the reason of the poor performance  
46 of these packed capillaries, more than on the kinetic performance of particles themselves,  
47 this could depend either on the difficulty of efficiently packing chiral core-shell particles  
48 (and thus to the contribution of eddy dispersion to peak broadening) or on the overall  
49 difficulty in getting efficient SPP columns at the capillary scale [13–19].

50 The most systematic work on the comparison between chiral FPPs and SPPs has been  
51 done by Armstrong's group [20–22]. With the aim of investigating the potential of chiral  
52 SPPs for ultrafast enantioseparations, Armstrong and coworkers characterized a wide  
53 variety of bonded brush-type CSPs prepared on 2.7  $\mu\text{m}$  SPPs, including cyclofructan-6  
54 based,  $\beta$ -cyclodextrin and macrocyclic antibiotics (in particular, teicoplanin, teicoplanin

55 aglycone and vancomycin) [20]. The concept that emerges from these studies is that chiral  
56 SPPs outperform their FPP counterparts in any chromatographic mode, namely, reversed-  
57 phase (RP), normal phase (NP), polar organic and HILIC.

58 In the first part of this paper, we report about the synthesis of novel Pirkle-type Whelk-  
59 O1 2.6  $\mu\text{m}$  chiral SPPs and the kinetic characterization of columns packed with these par-  
60 ticles. To this scope, a comparison between the performance of these columns and those of  
61 columns packed with both 2.5 and 1.8  $\mu\text{m}$  FPPs functionalized with identical chiral selec-  
62 tor [23, 24] was performed by using *trans*-stilbene oxide (TSO) enantiomers as probes. In  
63 the second part of the work, the potential of Whelk-O1 CSPs for ultrafast enantiosepara-  
64 tions on the second/sub-second time-scale is investigated by means of short columns (10  
65 mm packed with both FPPs and SPPs) operated at very high flow rates (up to 8 ml/min).

## 66 2. Experimental section

67 *Columns and materials.* All solvents and reagents employed in this work were purchased  
68 from Sigma-Aldrich (St. Louis, MI, USA). Kromasil silica (1.8 and 2.5  $\mu\text{m}$  particle size,  
69 100 Å pore size, 323  $\text{m}^2/\text{g}$  specific surface area) was from Akzo-Nobel (Bohus, Sweden).  
70 Whelk-O1 selector was generously donated by Regis Technologies Inc (Morton Grove,  
71 IL, USA). Accucore silica (2.6  $\mu\text{m}$  particle size, 80 Å pore size, 130  $\text{m}^2/\text{g}$  specific surface  
72 area, 0.5  $\mu\text{m}$  shell thickness) was from Thermo Fisher Scientific (Waltham, MA, USA). 150  
73 and 100 mm  $\times$  4.6 mm empty stainless steel columns were from IsoBar Systems by Idex  
74 (Erlangen, Germany), while 10  $\times$  4.6 and 10  $\times$  3.0 mm ones (including their holders) were  
75 fully developed and produced in-house. Fourteen polystyrene standards (from Supelco  
76 Sigma-Aldrich, Milan, Italy) with molecular weights 500, 2000, 2500, 5000, 9000, 17500,  
77 30000, 50000, 156000, 330000, 565000, 1030000, 1570000, 2310000 were employed for in-  
78 verse size exclusion chromatography (ISEC).

79 *Equipment.* Two chromatographic equipments were employed in this work. Unless dif-  
80 ferently specified, the UHPLC chromatographic system used for 150 and 100 mm columns  
81 was an UltiMate 3000 RS system from Thermo Fisher Dionex (Whaltam, MA, USA) con-

82 sisting of a dual gradient RS pump (flow rates up to 8.0 mL/min; pressure limit 800 bar  
83 under NP conditions), an in-line split loop Well Plate Sampler, a thermostated RS Column  
84 Ventilated Compartment and a diode array detector (UV Vanquish) with a low dispersion  
85 2.5  $\mu\text{L}$  flow cell. Detection wavelength was 214 nm (constant filter time: 0.002 s; data col-  
86 lection rate: 100 Hz; response time: 0.04 s). To reduce the extra-column contributions two  
87 350 $\times$ 0.10 mm I.D. Viper capillaries were used to connect the injector to the column and  
88 the column to the detector. The extra-column peak variance (calculated through peak  
89 moments) was 5.5  $\mu\text{L}^2$  in Hex/EtOH 90:10 + 1% MeOH at a flow-rate of 1.0 mL/min  
90 (extra-column volume: 12.2  $\mu\text{L}$ ). Data acquisition, data handling and instrument control  
91 were performed by Chromeleon (vers. 6.8) software.

92 An UPLC Acquity Waters system (Milford, MA, USA), equipped with a binary solvent  
93 manager (2mL/min maximum flow rate; pressure limit 1000 bar), an auto-sampler with a  
94 5  $\mu\text{L}$  injection loop, a thermostated column compartment (operated in still air conditions  
95 [5]), a diode array detector with a 500 nL flow cell, 80 Hz acquisition rate (resolution 4.8  
96 nm; no filter time constant) was employed. Two Viper capillaries (250 $\times$ 0.100 mm and  
97 350 $\times$ 0.100 mm  $L\times$ I.D.) were used as inlet and outlet connectors. The extra-column peak  
98 variance (through peak moments) was only 0.91  $\mu\text{L}^2$  at 1.0 mL/min. An updated version  
99 of Empower software was used in order to measure the second central time moments  
100 of the recorded concentration profiles. For the 10 mm columns, a modified version of  
101 the UPLC was used (Fig. S1 of Supplementary Data shows some images of the exper-  
102 imental arrangement). The programmable auto-sampler was replaced with an external  
103 in-house modified sample injector from VICI, Houston, TX, USA (model C74U). Essen-  
104 tially, this modification allowed for an electronic and fine control of the switching time  
105 (1.10 s) from injection to loading position and back. The injector is equipped with a 50  
106 nL internal injection loop and a micro-electric actuator (Valco instruments, Houston, TX,  
107 USA). The sample solution was introduced through a 25  $\mu\text{L}$  syringe. This arrangement  
108 ensured consistent reduction of tailing effect and high reproducibility between injections.  
109 The standard inlet and outlet connecting tubes were replaced by two PEEK tubings of, re-

110 spectively, 50 and 60 mm length  $\times$  63.5  $\mu$ m I.D. With this configuration, the extra-column  
111 peak variance (through peak moments) was only 0.14  $\mu$ L<sup>2</sup> at 1.0 mL/min.

112 *Synthesis of Whelk-O1 SPPs and preparation of columns.* Whelk-O1 SPPs were synthesized  
113 according to the procedure described by Pirkle and co-workers in 1992 [25, 26], which has  
114 been also employed for the synthesis of Whelk-O1 FPPs [27–29].

115 CHN elemental analysis for the different silica types functionalized in this work re-  
116 turned the following values: 6.28% C, 0.84% H and 0.73% N for 2.6  $\mu$ m SPPs; 13.41% C,  
117 1.73% H and 1.39% N for 1.8  $\mu$ m FPPs; 13.30% C, 1.73% H and 1.38% N for 2.5  $\mu$ m FPPs.  
118 Calculated bonding densities (based on N) are reported in Table 1. Details on how these  
119 calculations were performed can be found in reference [30]. FT-IR (KBr) of Whelk-O1  
120 were: 2924, 2864, 1675, 1627, 1548, 1513, 1344, 1078  $\text{cm}^{-1}$ .

121 All columns were slurry packed with a pneumatically driven Haskel pump ( $P_{max}$  =  
122 1000 bar). The slurry solution (10% w/v of Whelk-O1 particles in acetone) was pushed  
123 into the column by using a mixture of hexane/2-propanol 90:10 (% v/v) as pushing sol-  
124 vent. The pressure was increased from 400 bar up to 1000 bar. 100 mL of pushing solvent  
125 were pumped into the column at 1000 bar to consolidate the bed. Decompression until  
126 atmospheric pressure was gradually performed.

127 *van Deemter curve measurements.* The kinetic performance of Whelk-O1 columns was eval-  
128 uated in NP conditions. The mobile phase was a mixture of hexane/ethanol 90:10 (% v/v)  
129 + 1% methanol. Injection volumes were 0.1-0.5  $\mu$ L. Temperature was set at 35°C. Reten-  
130 tion time ( $t_R$ ) and column efficiency (number of theoretical plates,  $N$ ) of eluted peaks  
131 were automatically processed by the Chromeleon and Empower 3 software (using peak  
132 width at half height, according to European Pharmacopeia).  $N$  values were not corrected  
133 by extra-column contribution. The flow rates employed for studying the dependence of  
134 height equivalent to a theoretical plate  $H$  ( $=L/N$ , being  $L$  the column length) on the mo-  
135 bile phase velocity started from 0.1 mL/min up to maximum respectively of 4.0 mL/min  
136 (for 100 and 150 mm long columns; equipment: Dionex 3000RS) and 2.0 mL/min (for  
137 10 mm long columns; equipment: Waters Acquity), with constant steps of 0.1 mL/min.

138 van Deemeter curves were plotted as  $H$  vs. interstitial velocity,  $u_{int}$ .  $u_{int}$  was calculated  
139 according to the well known equation:

$$140 \quad u_{int} = \frac{F_v}{\pi r^2 \epsilon_e} \quad (1)$$

141 being  $F_v$  the flow rate,  $r$  the radius of the column and  $\epsilon_e$  the interstitial porosity.  $\epsilon_e$  was  
142 calculated by ISEC experiments, as described below.

143 *ISEC measurements, estimation of interstitial and total porosity and retention factor evaluation.*

144 ISEC measurements were performed by using tetrahydrofuran as mobile phase [31]. In-  
145 jection volume, flow rate and detection wavelength were, respectively, 2  $\mu$ L, 0.1 mL/min  
146 and 254 nm. For ISEC plots, retention volumes were corrected for the extra-column con-  
147 tribution before being plotted against the cubic root of the molecular weight ( $M_W$ ). The  
148 interstitial volume,  $V_e$ , was derived from the extrapolation to  $M_W = 0$  of the linear regres-  
149 sion calculated for the volumes of the totally excluded polystyrene samples [32]. From  
150 this, the estimation of external column porosity,  $\epsilon_e$ , is straightforward (being  $\epsilon_e = V_e/V_{col}$ ,  
151 with  $V_{col}$  the geometric volume of the column). The ISEC estimation of the thermody-  
152 namic void volume,  $V_0$ , was based on the retention volume of benzene. Through this, the  
153 total porosity  $\epsilon_t$  can be calculated ( $\epsilon_t = V_0/V_{col}$ ).

154 The retention factor for the  $i$ -th enantiomer,  $k_i$ , was calculated by:

$$155 \quad k_i = \frac{t_{R,i} - t_0}{t_0} \quad (2)$$

156 where  $t_{R,i}$  is the retention time of the  $i$ -th enantiomer ( $i = 1, 2$ ) and  $t_0$  the void time  
157 calculated by using carbon tetrachloride ( $\text{CCl}_4$ ) as marker.

158 *Specific permeability and Kozeny-Carman constant.* The specific permeability of each column  
159 was calculated according to the traditional equation [33, 34]:

$$k_0 = \frac{u\eta L}{\Delta P} \quad (3)$$

160 where  $u = F_v/\pi r^2$  is the superficial velocity and  $\eta$  the viscosity of the eluent (0.46 cP  
161 for THF at 25°C [35]).  $\Delta P$  is the difference between the total pressure drop,  $P_{tot}$ , and

162 the system pressure drop (without the column),  $P_{ex}$ .  $P_{ex}$  was measured by replacing the  
163 column with a zero-volume connector. Experimentally,  $k_0$  can be estimated by the slope  
164 of  $\Delta P$  vs.  $u$  plot [36].

165 The Kozeny-Carman constant  $K_c$  was estimated by [33]:

$$K_c = \frac{\epsilon_e^3}{(1 - \epsilon_e)^2} \frac{d_p^2}{k_0} \quad (4)$$

166 where  $d_p$  is the particle size (nominal  $d_p$ s given by manufacturer were used in this work  
167 in place of the more correct Sauter diameter value [5]).

### 168 3. Results and discussion

169 The preparation of SPPs was performed by following the same experimental protocol  
170 described in [27–29] for the functionalization of sub-2 $\mu\text{m}$  FPPs. The synthesis is partic-  
171 ularly advantageous and reproducible even on SPPs, since phenomena such as particle  
172 aggregation and clogging or the non-uniform/excessive selector coating, frequently en-  
173 countered with other chiral selectors, do not represent an issue with Whelk-O1 selector.  
174 Table 1 lists the characteristics of the particles employed in this work in terms of dimen-  
175 sion, specific surface area, pore size (data from manufacturers) and chiral-selector loading  
176 (see Experimental section). Surface coverage is given both as  $\mu\text{mol}$  per gram of bare sil-  
177 ica (column 6 of Table 1) and  $\mu\text{mol}$  per square meter (column 7). Several things can be  
178 observed from this table. The first is that the synthesis of FPPs of different dimensions is  
179 extremely reproducible (practically the same loading of chiral selector, about 390  $\mu\text{mol/g}$   
180 or 1.2  $\mu\text{mol/m}^2$ , was found on the 1.8 and 2.5  $\mu\text{m}$  FPPs). The second is that, by keeping  
181 constant the experimental conditions, functionalization of bare silica leads to significantly  
182 larger surface coverage of chiral selector (+ 20%) on SPPs (1.5  $\mu\text{mol/m}^2$ ) than on fully  
183 porous ones (1.2  $\mu\text{mol/m}^2$ ). This could be due to different reasons such as larger acces-  
184 sibility of external layers of particles, different surface chemistry of base silica FPPs and  
185 SPPs, etc. However, it is difficult to generalize these findings. They are indeed consistent  
186 with previous reports by Armstrong and coworkers [20, 21], but contrast with other data

187 from the same group [37]. Obviously, since the specific area per gram of FPPs is larger  
188 than that of SPPs, the total amount of chiral selector bounded per gram of base silica is  
189 also greater on the former type of particles than on fused-core ones.

190 The common understanding is that the larger the amount of chiral-selector tethered to  
191 the surface, the larger the loadability of the phase (which is definitely important in prepar-  
192 ative applications [38–40]) and the larger the retention factor. On the other hand, the rela-  
193 tionship between enantioselectivity and surface coverage of chiral selector is not straight-  
194 forward, since this last could impact also on the adsorption-desorption kinetics and thus  
195 on the separation efficiency. The resolution,  $R_s$ , of two chromatographic peaks (defined  
196 by the peak separation divided by the mean peak width) can be indeed expressed as [41]:

$$197 \quad R_s = \frac{\sqrt{N} \alpha - 1}{2} \frac{\bar{k}}{1 + \bar{k}} \quad (5)$$

199 where  $N$  is the number of theoretical plates, and  $\bar{k}$  and  $\alpha$  are, respectively, the average  
200 retention factor (i.e., the average of retention factors of the two enantiomers) and the  
201 selectivity, defined by [42]:

$$202 \quad \alpha = \frac{k_2}{k_1} \quad (6)$$

203 According to Eq. 5, one observes that resolution not only depends on the fact that solutes  
204 must be retained ( $\bar{k} \neq 0$ ) and that they must be retained at different extent ( $\alpha \neq 1$ ), but  
205 also on the efficiency of the column, with higher efficiencies giving better resolution.

206 Fig. 1 shows the chromatograms recorded for the separation of TSO enantiomers on,  
207 respectively, the 150×4.6 mm I.D. column packed with 2.5  $\mu\text{m}$  FPPs (top), the 100×4.6  
208 mm I.D. one packed with 1.8  $\mu\text{m}$  FPPs (middle) and, finally, the 150×4.6 mm I.D. column  
209 packed with 2.6  $\mu\text{m}$  SPPs (bottom). On each column, the flow rate (see figure caption)  
210 at which the chromatogram was recorded corresponds to the optimal flow rate, that is  
211 where the van Deemter curve presents its minimum (see later on). For the sake of com-  
212 parison between different columns, the x-axis is expressed as retention factor (in place  
213 of the traditional retention time). Retention factors were calculated by using  $\text{CCl}_4$  as the  
214 void volume marker (see the experimental section). As it can be noticed from Fig. 1, on

215 the two columns packed with 2.5  $\mu\text{m}$  and 1.8  $\mu\text{m}$  FPPs, TSO enantiomers are character-  
216 ized by the same retention factors ( $k_1 = 0.69$  and  $k_2 = 1.72$ ), with  $\alpha$  equal to 2.49. On  
217 the other hand, on the column packed with 2.6  $\mu\text{m}$  SPPs, retention of both enantiomers  
218 is smaller ( $k_1 = 0.50$  and  $k_2 = 1.27$ ) but  $\alpha$  is slightly larger (2.54). On the same figure  
219 the efficiency ( $N/m$ ) of each peak has also been reported.  $N$  was calculated as described  
220 in the experimental section. In all cases, very large values were observed. In particular,  
221 on the  $100 \times 4.6$  mm I.D. column packed with 1.8  $\mu\text{m}$  FPPs (middle chromatogram), an  
222 efficiency as large as 292,000 and 271,000  $N/m$  was obtained respectively for the first and  
223 the second eluted enantiomer. As a marginal remark, it can be observed that these values  
224 are typical of efficient RP systems [5, 36]. The resolution of columns, estimated by eq.  
225 5, resulted very large as well.  $R_s$  is 19.6 on the column packed with 1.8  $\mu\text{m}$  FPPs, 20.2  
226 for the column packed with 2.5  $\mu\text{m}$  FPPs and 17.3 on the column packed with core-shell  
227 particles. Therefore, the column packed with SPPs has the lowest  $R_s$ , even if the surface  
228 density of chiral-selector measured on these particles was the highest (Table 1). However,  
229 the overall much higher surface area for FPPs can outweigh this feature and explain this  
230 fact. The difference in  $R_s$  between columns packed with FPPs could reflect not only the  
231 difference in column length and thus in the total  $N$  per column (Fig. S2 of Supplementary  
232 Data graphically shows this concept by reporting, for the three columns,  $N$  per column  
233 as a function of velocity) but also the impact of particle size (1.8 vs. 2.5  $\mu\text{m}$ ) on the mea-  
234 sured efficiency. On the other hand, to explain the smallest  $R_s$  measured on the core-shell  
235 column one has to consider that the very favourable contribution of  $\alpha$  is ruled out by both  
236 the effect of efficiency and retention.

237 Table 2 reports some of the physico-chemical parameters in use to assess the quality  
238 of column packing, at least from a qualitative viewpoint, such as the external porosity,  $\epsilon_e$ ,  
239 and the Kozeny-Carman constant (see Eq. 4). For well packed columns,  $\epsilon_e$  is roughly 0.4  
240 [1, 43] and 0.37 [5, 44] respectively for beds made of core-shell and fully porous particles  
241 and the  $K_c$  constant is close to 180 [33]. As it can be seen from this table, for all columns  
242  $\epsilon_e$  was about 40%. However, while the columns packed with FPPs have  $K_c$  equal to 180,



243 for the one packed with SPPs  $K_c$  is only 160. For the sake of completeness, in Table 2, the  
244 total porosities,  $\epsilon_t$ , of columns are also reported (see the experimental section for details).  
245 Their values are close to typical values for columns packed with fully porous (0.65-0.7)  
246 and core-shell (0.52-0.55) particles [32, 39, 45].

247 The other important information that can be derived from Table 2 is about the per-  
248 meability (see Eq. 3) of columns. As expected, the column packed with  $1.8 \mu\text{m}$  FPPs is  
249 characterized by the smallest  $k_0$  value,  $2.95 \times 10^{-11} \text{ cm}^2$ , which reflects the difficulty of  
250 delivering a flow in a bed made of very fine particles. Surprisingly, the column packed  
251 with  $2.6 \mu\text{m}$  SPPs results to be about 25% more permeable than that packed with  $2.5 \mu\text{m}$  FPPs,  
252 even though their  $\epsilon_e$  are very similar. This could suggest a less dense packing of SPPs that,  
253 together with the already discussed low value of  $K_c$ , could affect the kinetic performance  
254 of the column.

255 When the van Deemter equation is employed in chiral chromatography, in addition  
256 to the traditional terms describing longitudinal diffusion ( $B$ ), eddy dispersion ( $A$ ) and  
257 solid-liquid mass transfer kinetics ( $C_S$ ), an additional term taking into account the slow  
258 adsorption-desorption kinetics ( $C_{ads}$ ), which frequently characterizes enantioselective  
259 phenomena, is also added [4, 46]. The dependence of  $H$  on the mobile phase velocity is  
260 therefore written as:

$$261 \quad H = A(u) + \frac{B}{u} + C_S u + C_{ads} u \quad (7)$$

262 Fig. 2 shows the van Deemter curves of TSO enantiomers measured, respectively, on the  
263  $150 \times 4.6 \text{ mm}$  column packed with  $2.5 \mu\text{m}$  FPPs (top), on the  $150 \times 4.6 \text{ mm}$  one packed with  
264  $2.6 \mu\text{m}$  SPPs (middle) and on the  $100 \times 4.6 \text{ mm}$  column packed with  $1.8 \mu\text{m}$  FPPs (bottom).  
265 Diamonds (green) refer to the first enantiomer and circles (blue) to the second one. The  
266 height equivalent to a theoretical plate has been plotted against the interstitial velocity,  
267  $u_{int}$  (Eq. 1), which represents the true linear velocity of the mobile phase (since the fluid  
268 flows around and between the particles, not through them). These plots suggest some  
269 considerations. First, one may observe that the longitudinal diffusion of the two enan-  
270 tiomers in each column is the same. This is demonstrated by the overlapping of their

271 van Deemter curves at low flow rates (where the  $B$ -term is dominant). Then, under the  
272 assumption of the same eddy dispersion for the two enantiomers in a given column [47],  
273 the conclusion is reached that the difference in the van Deemter curves (already evident at  
274 relatively low linear velocity, starting at  $u_{int}$  roughly 0.3 cm/s) is essentially due to a slow  
275 adsorption-desorption process. This is particularly evident for the column packed with  
276 2.6  $\mu\text{m}$  SPPs (middle plot). Another interesting observation coming from Fig. 2 is that the  
277 slope of the  $C$ -branch of the van Deemter equation is markedly steeper for the column  
278 packed with 1.8  $\mu\text{m}$  FPPs (bottom part of the figure) than for columns packed with both  
279 2.5  $\mu\text{m}$  FPPs (top) and 2.6  $\mu\text{m}$  SPPs (middle). This is due to frictional heating generated by  
280 the stream of mobile phase against the packed bed of the column through which it perco-  
281 lates under significant pressure gradient [48–50]. For instance, at  $u_{int}=0.8$  cm/s, the back-  
282 pressure generated by the 1.8  $\mu\text{m}$  column was 5300 psi and, at  $u_{int}=1.0$  cm/s, it reached  
283 6750 psi. The heat produced locally is dissipated in both the radial and longitudinal direc-  
284 tion of the column. This generates longitudinal and radial temperature gradients, whose  
285 amplitude depends on the degree of thermal insulation of the column (either adiabatic  
286 or isothermal). The column compartment of the Dionex UHPLC equipment used for the  
287 measurement of the van Deemter curves with these columns (see Experimental section)  
288 can only work in the so-called forced-air mode (quasi-isothermal conditions), where it is  
289 well known that radial temperature gradients degrade the efficiency of column [51–53].

290 With the purpose of comparing the behavior of the three columns, in Fig. 3 van  
291 Deemter curves of the first and the second TSO enantiomer are overlapped. Curves on  
292 top of this figure are those for the less retained enantiomer, while on the bottom there are  
293 the van Deemter curves relative to the second enantiomer. The kinetic behavior of the  
294 first enantiomer looks very similar on all columns, in consequence of the very low reten-  
295 tion (see Fig. 1) of this compound that does not allow to draw any significant conclusion  
296 on mass transfer phenomena. The only minor difference is around the minimum of van  
297 Deemter curves, where the core-shell column is the less efficient (see later on).

298 By considering the second enantiomer (bottom part of Fig. 3), very different kinetic

299 behaviors can be observed, depending on column. Unexpectedly, the column packed  
300 with Whelk-O1 2.6  $\mu\text{m}$  SPPs (circles, purple), no matter the flow rate, is characterized by  
301 the worst performance, even worse than its 2.5  $\mu\text{m}$  fully porous counterpart (diamonds,  
302 cyan). This is a surprising result that contrasts with the commonly observed performance  
303 of columns packed with  $\text{C}_{18}$  SPPs [6, 7]. It can be explained by considering the con-  
304 tribution to band broadening coming from either eddy dispersion or slow adsorption-  
305 desorption kinetics or a combination of both. The first statement, about the importance  
306 of eddy dispersion in columns packed with SPPs, is counter intuitive at least according to  
307 literature data that demonstrate how packed beds made of SPPs are expected to be more  
308 efficient than those of FPPs (see before). It can be however suggested by the experimen-  
309 tal difficulties encountered during the slurry packing of Whelk-O1 SPPs. By considering  
310 their characteristics, first of all that these particles are polar, however it does not seem  
311 weird that they behave differently from hydrophobic  $\text{C}_{18}$  ones during the slurry packing  
312 [19, 54]. As a matter of fact, not only the achievement of stable slurry suspensions was  
313 more difficult with very polar SPPs than with Whelk-O1 fully porous ones but also, e.g.,  
314 the time needed to compress the bed (by high-pressure flushing) did not follow any ex-  
315 pected trend and could not be optimized. In conclusion, the impression is that one of the  
316 most important characteristics of hydrophobic core-shell particles, i.e. their ability to gen-  
317 erate very efficient packed beds, could not be easily reproducible with very polar Whelk-  
318 O1 SPPs. Further investigation is needed to assess this point, in particular on rheological  
319 characteristics of Whelk-O1 SPPs. In agreement with [11, 12], it should be concluded that  
320 the efficient preparation of packed beds of polar SPPs still requires a long way to go. This  
321 essentially needs the optimization of all steps of packing protocol, without which the full  
322 potential of polar chiral SPPs can be barely reached.

323 As mentioned before, on the 2.6  $\mu\text{m}$  Whelk-O1 core-shell column the contribution  
324 to band broadening coming from a slow mass transfer process seems to be particularly  
325 evident. Since the solid-liquid mass transfer term ( $C_s$ ) should be lower on core-shell than  
326 on fully porous particles (due to the presence of the inaccessible core), the conclusion

327 is that the adsorption-desorption kinetics must be slower on core-shell particles (higher  
328  $C_{ads}$  term in eq. 7) than on the fully porous ones. An explanation could be the different  
329 surface density of chiral selector between core-shell and FPPs. Table 1 shows that this  
330 surface density is about 20% larger on SPPs than on fully porous ones. In literature there  
331 are practically no studies which have attempted to assess if and how chiral recognition  
332 is modified by changing the amount of chiral selector tethered to the surface and how  
333 this could impact on the chromatographic performance [12]. On the other hand, this is  
334 a very important subject that needs more experimental and theoretical work to be fully  
335 understood.

336 Finally, by still looking at the bottom part of Fig. 3, it is evident that the column  
337 packed with 1.8  $\mu\text{m}$  FPPs (triangles, green) outperform the other two in terms of kinetic  
338 behavior but it is also clear that, at high flow rates, where the effect of frictional heating  
339 on efficiency is dominant, this column does not offer any advantage over the one packed  
340 with 2.5  $\mu\text{m}$  FPPs. Indeed, at  $u_{int}$  slightly larger than 1 cm/s, the C-branch of the 1.8  $\mu\text{m}$   
341 fully porous column merges to that of the column packed with 2.5  $\mu\text{m}$  FPPs.

342 Fig. 4 (top) shows the gain in analysis time that can be obtained by moving from  
343 both the columns packed with 2.5  $\mu\text{m}$  FPPs and 2.6  $\mu\text{m}$  SPPs to that packed with 1.8  $\mu\text{m}$   
344 FPPs. The necessary premise to discuss this figure – whose meaning is merely practical –  
345 is that the length of commercially available columns packed with 2.5-2.7  $\mu\text{m}$  particles (no  
346 matter if fully porous or pellicular) is usually 150 mm, while that of columns packed with  
347 sub-2 $\mu\text{m}$  particles is only 100 mm or less. This justifies the direct comparison presented  
348 in Fig. 4, where column length is not accounted for. Having acknowledged this, and  
349 by referring for each column to condition of maximum efficiency (indeed chromatograms  
350 presented in Fig. 4 were recorded at the optimum flow rate, see figure caption for details),  
351 one observes that the column packed with 1.8  $\mu\text{m}$  FPPs permits to decrease analysis time  
352 (here simply calculated as the retention time of the second eluted enantiomer) more than  
353 50 and 30% with respect to the 2.5  $\mu\text{m}$  fully porous column and the 2.6  $\mu\text{m}$  core-shell  
354 one. The practical advantage achievable with the 100 mm column packed with sub-2 $\mu\text{m}$

355 particles, becomes still more evident by considering, in addition to analysis time, also the  
356 resolution of columns (see before). Thus, the ratio between resolution and analysis time  
357 [55], graphically given as bar chart in the bottom part of Fig. 4, is strongly favorable for  
358 the 1.8  $\mu\text{m}$  column packed with FPPs (it is indeed 11.9 on this column vs. 5.3 and 7.9  
359 on, respectively, the 2.5  $\mu\text{m}$  fully porous and the 2.6  $\mu\text{m}$  core-shell column). Incidentally,  
360 the gain of  $R_s/t_{R,2}$  ratio observed for the 2.6  $\mu\text{m}$  core-shell column over that packed with  
361 2.5  $\mu\text{m}$  FPPs comes from the reduction of retention time in the former column (due to a  
362 much lower total surface area per column) and not from an increase of  $R_s$  (which actually  
363 is larger on the 2.5  $\mu\text{m}$  fully porous column).

364 The last part of this study briefly reports on the use of short columns, packed with  
365 both Whelk-O1 FPPs and SPPs, to realize ultrafast enantioseparations. In this proof-of-  
366 concept study, 10 mm columns of different I.D. (3.0 and 4.6 mm) were employed. These  
367 columns were in-house designed and developed. Fig. S3 of Supplementary Data shows a  
368 picture of the 10 mm column and holder. They were packed by following the same proto-  
369 col also used for longer columns. Table 3 has some information that helps to characterize  
370 these columns, in particular the optimal flow rate (i.e., the flow rate corresponding to the  
371 minimum of van Deemter curve), the corresponding interstitial linear velocity and the  
372 maximum efficiency (in  $N/m$ ). With the purpose of performing ultrafast enantiosepara-  
373 tions, these columns were operated at the maximum flow achievable by instrumentation  
374 (8 ml/min). Accordingly, the Thermo Dionex equipment (see experimental section) was  
375 employed, even though its extra-column variance is not negligible with respect to that of  
376 first and second eluted enantiomers (respectively, roughly 11.2 and 28  $\mu\text{L}^2$ ). In the last  
377 column of Table 3, the number of theoretical plates per column measured at the highest  
378 flow rate is reported. As an example, Fig. 5 shows the chromatogram recorded with the  
379 10 $\times$ 3.0 mm column packed with 1.8  $\mu\text{m}$  FPPs. As it can be seen, the separation of TSO  
380 enantiomers was performed in less than 1 s, with  $R_s = 2.2$ . This represents an extraordi-  
381 nary result, unimaginable only a few years ago in chiral liquid chromatography, which is  
382 even comparable with that of chiral separations on microchip platforms [56].

#### 383 4. Conclusions

384 The investigation of the kinetic performance of columns packed with Whelk-O1 fully  
385 porous and core-shell particles of similar diameter ( $2.5\ \mu\text{m}$  for FPPs vs.  $2.6\ \mu\text{m}$  for core-  
386 shell ones) has surprisingly revealed that FPPs outperform SPPs. This depends, in part,  
387 on the faster mass-transfer adsorption-desorption kinetics observed (especially on the  
388 second eluted enantiomer) on the FPPs and, in part, on the smaller eddy dispersion con-  
389 tribution to band broadening on the column packed with FPPs. The slower mass-transfer  
390 adsorption-desorption process is most likely due to the larger surface density of chiral  
391 selector on the SPPs. Indeed, even though the same experimental conditions were main-  
392 tained during functionalization of SPPs and FPPs, the outcome was different. The surface  
393 density of Whelk-O1 selector on SPPs was indeed 20% larger than that of FPPs. These  
394 results suggest that, at least for the case considered in this work, the higher the surface  
395 coverage, the lower the adsorption-desorption process but with the information in our  
396 possession no generalization can be made. Fundamental studies aimed at investigating  
397 the relationship between mass transfer kinetics and surface density of chiral selector are  
398 needed.

399 On the other hand, the empirical difficulty to pack Whelk-O1 core-shell particles ex-  
400 plains the important eddy dispersion contribution to band broadening in columns packed  
401 with these particles. Different attempts have been done to improve the packing process,  
402 by varying many experimental variables (slurry composition, consolidation time, etc.)  
403 during the packing, but without success. These findings show that packing polar SPPs is  
404 significantly different from packing hydrophobic SPPs (such as  $\text{C}_{18}$  particles), for which  
405 a large amount of information and expertise has been collected over the years. One of the  
406 most significant characteristics of beds made of  $\text{C}_{18}$  core-shell particles is their extremely  
407 low eddy dispersion term. This, however, seems to be difficult to achieve with Whelk-O1  
408 SPPs. The investigation of rheological properties of these particles can help to understand  
409 their different behavior with respect to fully porous particles so to optimize the packing  
410 protocol and, thus, the kinetic performance of columns made of polar Whelk-O1 SPPs.

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416 The authors thank Thermo Fisher for providing Accucore 2.6  $\mu\text{m}$  SPP silica.

## 417 **Appendix A. Supplementary Data**

418 Supplementary data associated with this article can be found in the online version.

## 419 6. Figures and Tables

### 420 Figure captions

421 **Fig 1.** Chromatograms showing the separation of TSO enantiomers on the three columns  
422 employed in this work. Carbon tetrachloride was used as dead time marker. Top: 150×4.6  
423 mm column packed with Whelk-O1 2.5  $\mu\text{m}$  FPPs; middle: 100×4.6 mm column packed  
424 with Whelk-O1 1.8  $\mu\text{m}$  FPPs; bottom: 150×4.6 mm column packed with Whelk-O1 2.6  
425  $\mu\text{m}$  SPPs. Chromatograms were recorded at the flow rate corresponding to the minimum  
426 of the van Deemter curve (they were, from top to bottom, respectively 1.2, 1.8 and 1.5  
427 ml/min). For the sake of comparison, x-axis is given in terms of retention factor instead  
428 of retention time. Close to each peak, efficiency ( $N/m$ ), retention factor ( $k$ ) and retention  
429 time ( $t_R$ ) are indicated. Instrument employed for measurements: UPLC Waters Acquity.

430

431 **Fig 2.** van Deemter curves for TSO enantiomers measured on Whelk-O1 columns (same  
432 geometries as in Fig. 1) packed with, respectively, 2.5  $\mu\text{m}$  FPPs (top), 2.6  $\mu\text{m}$  SPPs (mid-  
433 dle) and 1.8  $\mu\text{m}$  FPPs (bottom). Instrument employed for measurements: Dionex 3000RS.

434

435 **Fig 3.** Overlapped van Deemter curves measured on the three Whelk-O1 columns (same  
436 geometries as in Fig. 1), respectively for the first (top) and the secondly (bottom) eluted  
437 TSO enantiomers. Diamonds: column packed with 2.5  $\mu\text{m}$  FPPs; circles: column packed  
438 with 2.6  $\mu\text{m}$  SPPs; triangles: column packed with 1.8  $\mu\text{m}$  FPPs. Instrument employed for  
439 measurements: Dionex 3000RS. See text for details.

440

441 **Fig 4.** A) Same chromatograms as in Fig. 1, showing the separation of TSO enantiomers  
442 on the three columns employed in this work, but with the x-axis given in retention time.  
443 Carbon tetrachloride was used as dead time marker. B) Bar chart showing the ratio be-  
444 tween resolution and retention time for the 2.6  $\mu\text{m}$  core-shell column (first bar on the left,  
445 blue color), the 1.8  $\mu\text{m}$  fully porous column (middle bar, orange) and, finally, the 2.5  $\mu\text{m}$



446 fully porous column (last bar on the right, red). Ratios were calculated on the second  
447 eluted enantiomer. Instrument employed for measurements: UPLC Waters Acquity.

448

449 **Fig 5.** Example of ultrafast enantioseparation thanks to the use of short column and high  
450 flow rate. In this particular case, a 10×3.0 mm column packed with 1.8 μm FPPs was  
451 operated at 8 ml/min ( $u_{int} = 4.8$  cm/s) for the separation of TSO enantiomers. Carbon  
452 tetrachloride was used as dead time marker. Note the time scale in seconds. Instrument  
453 employed for measurements: Dionex 3000RS. See text for details.

454

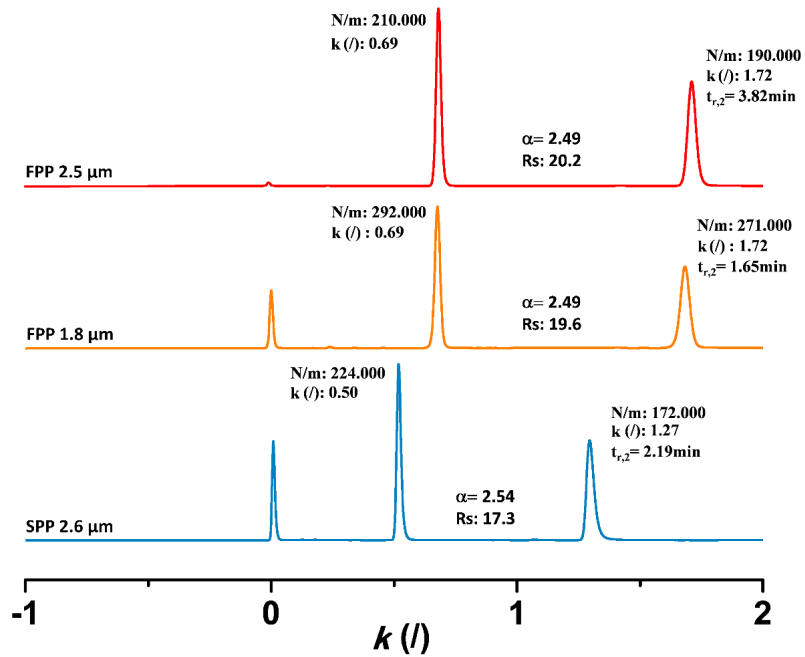


Figure 1:

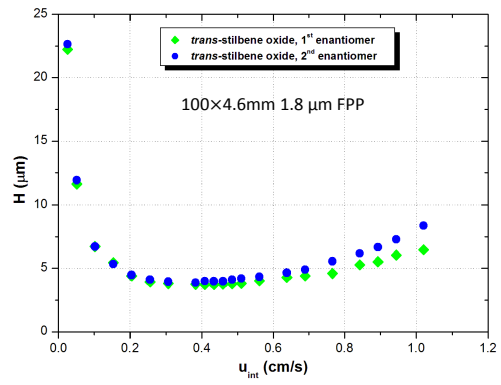
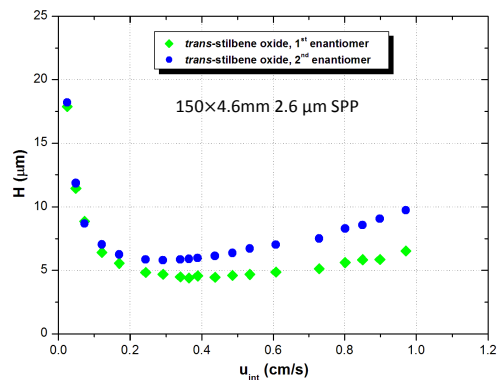
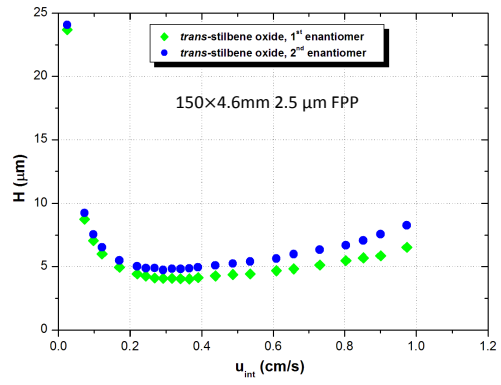


Figure 2:

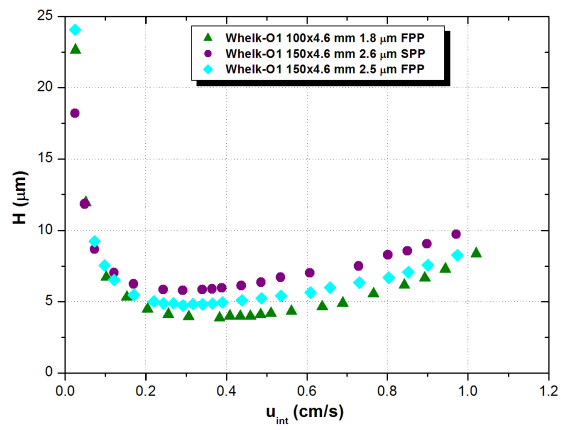
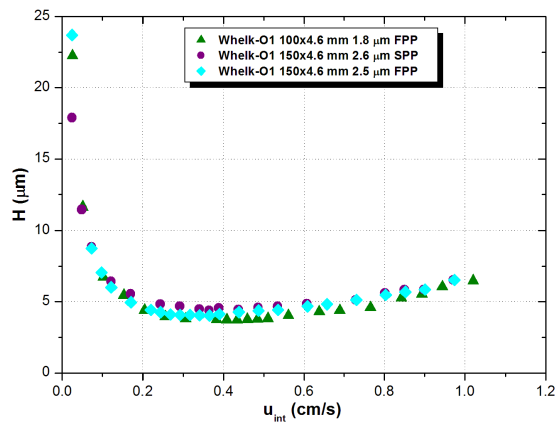


Figure 3:

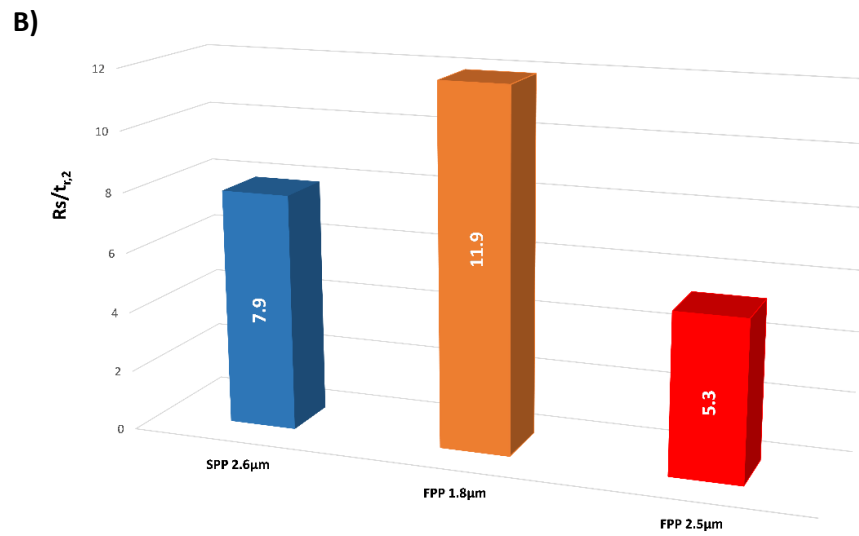
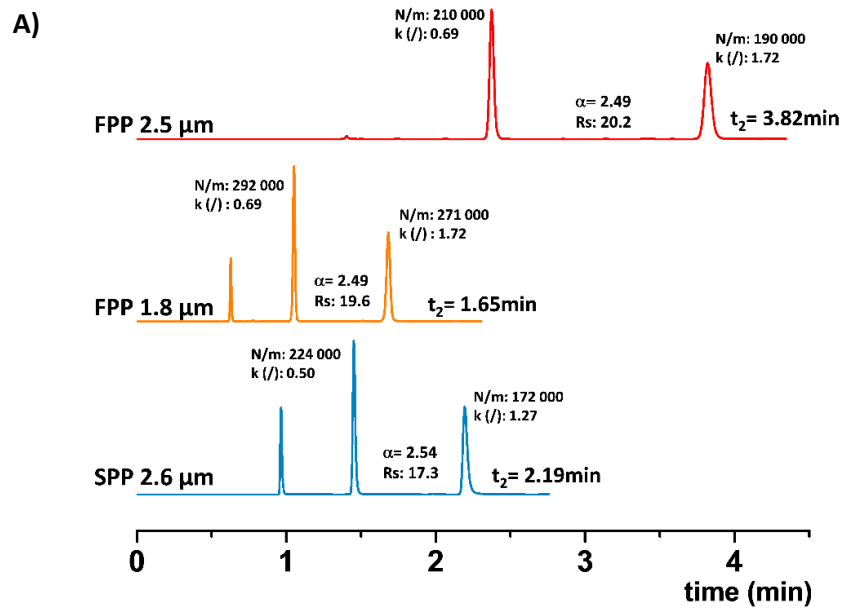


Figure 4:

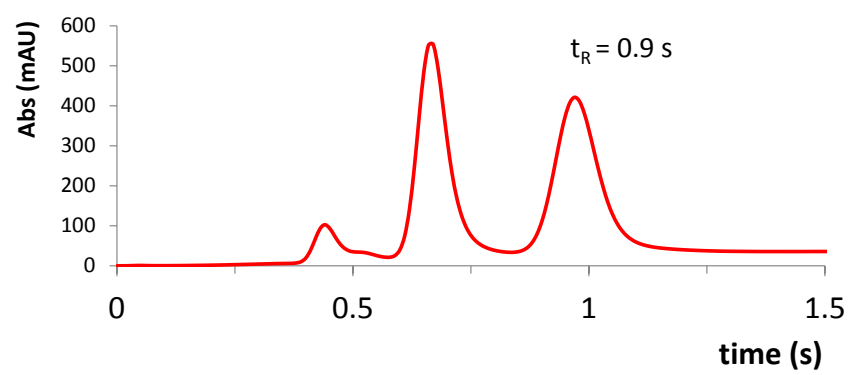


Figure 5:

Table 1: Geometrical characteristics of Whelk-O1 columns: particle type (FP: fully porous, SP: superficially porous); column dimensions; particle diameter ( $d_p$ ); specific surface area ( $A_s$ ); pore size; bonding density (given both as  $\mu\text{mol}$  per gram of bare silica and  $\mu\text{mol}$  per square meter).

Particle type	Dimensions	$d_p$	$A_s$	Pore size	Bonding density	
	(L×I.D., mm)				( $\mu\text{m}$ )	( $\text{m}^2/\text{g}$ )
FP	150×4.6	2.5	323	100	391.2	1.21
FP	100×4.6	1.8	323	100	394.6	1.22
SP	150×4.6	2.6	130	80	189.8	1.46

Table 2: Physico-chemical properties of Whelk-O1 columns: particle type (FP: fully porous, SP: superficially porous); total porosity ( $\epsilon_t$ ); external porosity ( $\epsilon_e$ ); Kozeny-Carman constant ( $K_c$ ); permeability ( $k_0$ ).

Particle type	$\epsilon_t$	$\epsilon_e$	$K_c$	$k_0 \times 10^{11}$ (cm <sup>2</sup> )
FP	0.670	0.412	180	7.06
FP	0.644	0.393	180	2.95
SP	0.524	0.413	160	8.60



Table 3: Kinetic performance (in  $N/m$ ) of short columns (10 mm) of different diameter.  $F_{v,opt}$  and  $u_{int,opt}$  represent, respectively, the optimum flow rate (that is the flow rate corresponding to the minimum of the van Deemter curve) and the optimum interstitial velocity;  $N_{max}$  is the number of theoretical plates per column, when the column was operated at 8 ml/min (see text for more details). In all cases,  $N$  has been calculated as the average value of  $N_s$  of the two TSO enantiomers. Particle type: FP, fully porous; SP, superficially porous). Instruments employed for measurements: UPLC Waters Acquity for van Deemter curves; Dionex 3000RS for ultrafast enantioseparations (evaluation of  $N_{max}$ ).

Particle type	L×I.D. (mm)	$F_{v,opt}$ (mL/min)	$u_{int,opt}$ (cm/s)	$N/m$	$N_{max}$
FP	10×4.6	1.7	0.43	190,000	1220
SP	10×4.6	1.5	0.36	140,000	850
FP	10×3.0	0.7	0.42	180,000	520

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