1	Electrical properties speculation of contamination by water and gasoline on sand
2	and clay composite
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11	ABSTRACT
12	Effects of temperature, frequency, and molarity on electrical conductivity
13	have been studied for sand-clay samples contaminated by water and gasoline.
14	Electrical properties changes according to frequency, contaminant type and
15	structure of components at the sample. A comparison was performed for these
16	contaminated sand-clay samples. Changes of dielectric constant (\in') ,
17	conductivity (σ) and complex impedance with frequency (0.1 Hz 2×10 ⁷ Hz),
18	with different contaminant concentration (at constant room temperature $\sim 21^{\circ}$ C)
19	have been studied. The sand-clay samples were mutually wetted gradually
20	using gasoline and distilled water. Then, electrical properties were measured
21	sequentially. Water is a conductive liquid and the contaminant gasoline is an
22	insulator. The experimental results indicate that, conductivity of samples
23	increases with increase of water concentration while with the additions of the

contaminant gasoline, the sample conductivity decreases. The permittivity, decreases with reduction of conductive links between grains and with the progressive increase of frequency. The conduction of electrical conductivity, commonly, increases with increase of connectivity between different links between grains. Also, conduction increases with progressive increase of frequency. Comparison of both outcomes from lab electrical measurements gives a speculation about the picture in the field.

Keywords: Electrical properties; conductivity; water saturation; gasoline
saturation; permittivity; frequency.

33

INTRODUCTION

There are many physical, chemical and mechanical properties that can 34 affect the electrical properties. These parameters may be grain shape, size, 35 orientations, interface boundaries, porosity, inhomogeneity, combination made 36 by mixing substances together, and structural interconnected pores of the 37 conducting and insulating fractions of the grains ... etc. Also, wetting the 38 samples with liquid is an efficient factor for the changing of electrical 39 characteristics (Gomaa and Abou El-Anwar 2015). The systematic 40 investigation of ac conductivity at various temperatures and frequencies gives 41 valuable information on conduction mechanisms at samples according to its 42 electric charge carriers (Gomaa 2013). In general, the gradual additions of 43 conductor concentration raise the conductivity value (Abou El-Anwar and 44 Gomaa 2016). Also, the gradual additions of conductor concentration decrease 45 the distance spaces separating two grains and, accordingly, raises the 46

permittivity values (Gomaa and Elsayed 2009). The latter increase of
conductivity and permittivity is present until the samples reach the percolation
concentration threshold (Gomaa 2008). Percolation threshold of concentration
is the conductor concentration fraction that permits complete contact between
electrodes.

52 Increase of conductivity is the outcome of growing of uninterrupted conduction links of conducting elements (water). The conduction values of 53 54 conductivity are faint at relatively low overall conductor amount. With progressive increase of overall conductor amount the conductivity becomes 55 greater (Gomaa et al. 2018, Gomaa and Kassab 2017). Generally, with increase 56 57 of overall conductor amount and with progressive increase of frequency more 58 continuous conductor links start to be established between the different grains (Gomaa et al., 2009). Increase of continuous conductor links leads to the 59 general increase of conductivity values (Knight and Endres 1990). The raise of 60 frequency initiates particles to overcome energy barriers between atoms and 61 therefore the conductivity value is increased. The growing of frequency makes 62 the permittivity decreases. Also, decrease of permittivity is initiated from 63 decrease of conductor concentration. When the conductor concentration 64 decreases, this leads, generally, to increase of insulator material along the 65 space separating the conducting grains. Permittivity values increase with 66 increase of total conductor concentration until it achieves the dispersion limit. 67 At that limit, the permittivity may decrease again above that percolation limit 68 (Gomaa and Alikaj 2009, Gomaa and Abou El-Anwar 2017). The small pores 69

among grains result in relative decrease of permittivity in samples 70 (Barabanova et al. 2013). Permittivity changes from one specimen to another 71 due to alteration of combinations, volumes and amounts of the conducting and 72 73 insulating materials in specimen. Also, there may be the texture between grains (Gomaa et al., 2015 a and b). Conductivity, in general, has a monotonic 74 75 attitude of increase with the successive increase of frequency. The permittivity, 76 in general, has a tendency to increase with decrease of the frequency (Kassab 77 et al. 2017, Gomaa 2006).

Frequency behavior of conductivity is may resulted from orientation and translational hopping mechanisms. Orientation mechanism means hopping and jumping of electron in the space separating two charged defects. The translation hopping means that there is D C conductivity at zero frequency. Imaginary impedance, which depends on frequency, point to the existence of different reactions in the system.

Comparing effect of water as a conductor and that of gasoline as an 84 insulator, with both frequency and wetting at lab was done in this work. To 85 achieve this study, a sand-clay sample was measured (electrically) at 86 laboratory. The samples was measured dry and at different contamination 87 saturations, of water and gasoline, at constant room temperature (~21 °C), at 88 frequency range of (0.1 Hz up 2×10^7 Hz). Electrical measurements; 89 permittivity, conductivity and complex impedance compared to frequency, 90 declare effect of contaminants and texture on the studied samples. The water is 91 conductive liquid, because miscibility of salts found in its structure and the 92

gasoline is insulator (Abou El-Anwar and Gomaa 2013). In the laboratory,
conductivity of samples increases with sample's water content while with
additions of gasoline the sample conductivity decreases. Wetting the samples
with liquid is effective factor in the change of electrical responses (Gomaa and
Kassab M., 2016).

In the current paper we will compare both outcomes from electrical measurements from different contaminants (water and gasoline) and we will discuss wetting conditions of water, gasoline and frequency on electrical laboratory measurements.

102

Experimental Details

103 Electrical measurements

104 Dielectric was measured using broadband dielectric spectrometer concept, Novo Control, Germany, at wide frequency range (0.1 Hz 2×10^7 Hz). We 105 apply testing voltage of 1 Vrms at constant room temperature (~21 °C). Sample 106 constituents are some small sand grains that are naturally mixed with some clay 107 impurities. The disc shaped sample holder has dimensions of 8 mm diameter 108 and 3.623 mm height with total volume of 0.182 cm^3 . Data were automatically 109 measured and studied by the instrument software WinDeta. The sample was 110 enclosed between two copper electrodes and a Teflon cylinder. The sample 111 then placed in its proper position inside the instrument. Measurements were 112 done in a row, pure sand-clay mixture and then 10 µL of filtered water or 113 gasoline was added to sample and measurement repeated. The last step was 114 repeated until the water volume in the specimen reaches 60 µL of filtered 115

116 water. The sample sand cell is present at Fig. (1), 1: is the Teflon cylinder and 117 2: indicates the two copper electrodes. Dielectric constant was calculated by the 118 formula $\in' = \frac{C_p d}{\epsilon_0 A}$ (Jonscher 1973, 1975, 1977 and 1999, Hill and Jonscher 119 1983). The ac conductivity is given by $\sigma = w \in ' \in_0$ (Hill and Jonscher 1983),

120 where w is the angular frequency.

121

122 **Results and Discussion**

123 Electrical properties of any mixture of samples are affected by:

124 1- The change of sample arrangement during pumping of the water or 125 gasoline. This may render inaccurate measurements as the field sample has 126 changed in its structure. This gives misleading data. Consequently, it would be 127 better to remove washout of the measured samples.

128 2- Using samples of large volume is suitable for electrical field 129 measurements. However, this may contradict the condition for laboratory 130 electrical measurements which is instituted on using of small volumes with 131 large areas. Physically, the laboratory sample must have small thickness to 132 form electric field with proper strength to minimize errors.

133

1) Chemical assembly of gasoline

Gasoline is a reiterated component of a liquid mixture of hydrocarbons. It is consisted of mixtures of hydrocarbons, blending agents, and additives. Commonly, the chemical constituents of gasoline hydrocarbons changes extensively (IARC 1989). This dependence is affected by crude oils concentrations, the filter procedure used, and the product precise requirement.

139 The gasoline composition range from 6 to 13 % of alkanes; 25 to 40 % iso-

alkanes; 3 to 7 % cyclo-alkanes; 1 to 4 % cyclo-alkenes; and from 20 to 50 % of

141 overall aromatics (0.5-2.5% benzene). Detailed information regarding the

142 Chemical analysis, particle size analysis, hydrogeological properties are located

143 at Table (1). The sand used is identified by the properties at Table (1).

144

Table 1 - Chemical analysis, Particle size analysis, Hydrogeological properties

Chemical analysis results										
	SiO ₂	TiO ₂	Al_2O_3	MnO	Fe ₂ O ₃	MgO	CaO	Na ₂ O	K ₂ O	CO_2
%	81.17	0.06	4.75	0.05	0.56	0.13	6.67	0.83	1.15	4.02
Partic	Particle size analysis of sand									
d (mn	u) 0 - 0.074		0.75 - 0.104	0.105-0.149		074.0 -061.0	0.421 - 0.840	0.841 - 2.000		>2.001
%	0.8	0	.03	0.20	14.	27	70.67	10.6	6	3.43
Hydrogeological properties										
d (mm)		K	K_{max} (m/s)		ρ (%)					
0.09			5*10 ⁻³			35				

145

146 2) Laboratory electrical measurements

147	Figure (2) shows the series resistance (R_s) with frequency spectrum and
148	distinct concentrations of filtered water (10 µL, 20 µL, 30 µL, 40 µL, 50 µL
149	and 60 μ L). The dry sand-clay samples have the highest resistance (Song et al.
150	1986, Leroy et al., 2008, Chew and Sen 1982, Chelidze and Guéguen 1999).
151	With the consecutive changes of disttled water, the resistance decreases. Series
152	resistance steeps down when adding the 1^{st} and 2^{nd} successive additions of
153	disttled water. The decrease is slowly with the 3 rd , 4 th and 5 th successive
154	additions. The last successive addition, 6 th dose, had a mild decrement reaching

minimum values of sreries resistance for sand-clay composite (e.g. Chelidze et 155 al. 1999, Sen 1984, Sen 1981, Olhoeft 1977). This is nearly the full saturation 156 of sand-clay sample. The sample series resistance descended three decades 157 with successive additions from dry to full saturation (Shaltout et al, 2012, 158 Gomaa 2009). When specimen is dry $(0 \ \mu L)$, decrease of the resistace value 159 with frequency is fast and requires nearly more than one decade for the whole 160 frequency range (Olhoeft 1976, Olhoeft 1980, Olhoeft 1985). When specimen 161 162 is wetted with the other successive additions of water (10 μ L, 20 μ L, 30 μ L, 40 μ L, 50 μ L and 60 μ L), decrease of the resistace with frequency is slow and 163 takes nearly half decade in the whole frequency range (Minaw et al. 1972, 164 165 Levitskaya and Sternberg 1996 a, b, Levitskaya 1984).

166 The dry sample does not reach saturated (flat) resistance value, even at very high frequency (2×10^7 Hz), while the other wet samples (10 μ L, 20 μ L, 167 30 μ L, 40 μ L, 50 μ L and 60 μ L) reaches the saturated (flat) resistance value at 168 relatively lower frequencies (10^3 Hz), and differs gradually from one saturation 169 to the other (Gomaa and Elsayed 2006, Gomaa et al. 2000). As the satuartion 170 171 concentration increases, the saturated (flat) resistance value at definite 172 frequency is decreased (Mendelson and Cohen 1982, Last and Thouless 1971, 173 Knight and Nur 1987). The sample series resistance nearly takes three decades 174 from the dry condition to the full saturation in the whole frequency range.

Figure (3) displays the series resistance (R_s) with frequency dry and at various saturations of gasoline. The dry sand-clay samples have the lowest resistance. Series resistance (R_s) increases with adding gasoline concentrations

 $(10 \ \mu\text{L}, 20 \ \mu\text{L}, 30 \ \mu\text{L}, 40 \ \mu\text{L}, 50 \ \mu\text{L}$ and $60 \ \mu\text{L}$). Subsequent gasoline additions 178 are quite different from water additives. The series resistance is directly related 179 to gasoline addition. However, the whole of growth of the series resistance was 180 within one decade at the whole frequency range. Series resistance raised with 181 raise of gasoline concentration (Jonscher 1973, 1975, 1977 and 1999, Hill and 182 Jonscher 1983). The dry sample has very low resistance while successive 183 gasoline concentration increases the resistance sequentially. The series 184 185 resistace of the dry sample $(0\mu L)$ decreases with frequency increase (Garrouch and Sharma 1994, Dias 2000, Chinh 2000). The variation of the series 186 resistance, nearly, takes more than one decade in the whole frequency range. 187 When specimen is contaminated with gasoline (10 μ L, 20 μ L, 30 μ L, 40 μ L, 50 188 μ L and 60 μ L), the resistace is higher. Resistace is raised with raise of the 189 gasoline concentration with more faster degree (with frequency), consuming 190 nearly two decades in the whole frequency range for high concentration (60 191 μL). All samples does not accomplish saturation resistance of frequency even 192 at very high frequency (2×10^7 Hz). The curves will not reach that saturation 193 194 resistance frequency (with frequency increase, the resistance is still decreasing, 195 Chelidze 1979, Knight and Abad 1995). Clear difference is found between the series resistace value at Fig. (2) (2X10⁵) for high water saturation and that 196 value of series resistace at Fig. (3) (1X10⁶) for high gasoline saturation. This 197 198 difference is completely attached to change of the contaminent (Bussian 1983, Khalafalla and Maegley 1973). The gasoline saturation is quitely increases the 199 resistance and water saturation is quitely decreases the resistance. 200

Fig. (4) Shows the permittivity (ε') with frequency dry and at various 201 concentrations of filtered water (10 µL, 20 µL, 30 µL, 40 µL, 50 µL and 60 202 μ L). The successive additions of water concentrations increases the value of 203 sample permittivity by nearly one decade, at low frequency, and this value 204 decreases at relatively high frequency. At low frequency, permittivity (ε ') has 205 relative high values that decrease with frequency increase and finally at 206 relatively high frequencies becomes independent of frequency. The the 207 permittivity decreases rapidly at relatively lower frequencies and decreases 208 relatively higher frequencies. slowly at Normal permittivity (ε') 209 behaviourshow that there values decreases with increasing frequency untell it 210 reacches a constant value. Above definite frequency range, the exchange 211 interaction of electron between the ions cannot keep track of applied electric 212 field. At relatively high frequency regions, the charge carriers would barely 213 have started to move before the field reversal occurs and the permittivity ε' 214 falls to its smallest values. Space charge polarization arises between grain 215 interfaces and grain-electrode interface due to inhomogenety of permittivity 216 structure at these interfaces. This is what is called double layer; semi-217 conducting grains separated by insulating or poor conducting grains. The 218 permittivity of a material comes from electronic, ionic and space charge 219 220 accumulation. The electronic contribution is the main factor that are affected by the present frequency range, while at other frequency ranges other mechanisms 221 may be the dominant factors. 222

Figure (5) Shows the permittivity (ε ') with frequency, dry and at various saturations of gasoline. The successive additions of gasoline decreases the value of sample permittivity by less than one decade, for lower frequency ranges.

Figure (6) shows the complex series impedance (Z_s) for the sand-clay 227 sample dry and at various concentrations of filtered water (10 µL, 20 µL, 30 228 229 μ L, 40 μ L, 50 μ L and 60 μ L). For the dry condition case, measured impedance 230 shows nearly an arc (or a part of another semicircle, for lower frequencies) in contact with another semicircle (at relatively higher frequency). This indicates 231 232 two different polarization mechanisms within the specimens. First semicircle 233 (at high frequency) shows the properties of specimen materials (bulk property). 234 The other arc or the other part of semicircle (at low frequency) shows the 235 properties of interface (grain boundary) between the grains. This may be 236 resulted from transport of charges across the grain boundaries. Complex impedance was gradually decreasing with frequency increase which resulted 237 238 from space charge increase at relatively higher frequencies. With increase of 239 conductor concentration (distilled water), the relaxation peak proceeds to higher frequency and its strength decreases. This effect that is similar in 240 behaviour, more or less, to rise of temperature. 241

Figure (7) shows the complex parallel impedance (Zp) for the sand-clay samples, dry and at various saturations of gasoline (10 μ L, 20 μ L, 30 μ L, 40 μ L, 50 μ L and 60 μ L). For dry sample, measured impedance plane shows nearly an arc (at low frequency) that has low impedance than the other

saturated curves. This arc describes the total conductor connections at the 246 specimen. Also, we can find two different polarization mechanisms within the 247 samples (bulk at relatively higher frequency and grain boundary at relatively 248 low frequencies). As gasoline concentration increases, the impedance peaks 249 move to high values of complex impedances. Also, sequential additions of 250 251 gasoline concentrations cause the peaks widths to be broader and more 252 expanded. The expansion of peaks means that the barriers that the ions have to 253 overcome, due to increment of resistivity, become bigger with the additions of gasoline concentrations. As insulator contaminant increases (gasoline), the 254 255 relaxation peak proceeds to lower frequencies and increases in its strength and 256 become broader.

Figure (8) displays the Nyquist representation of conductivity of sandclay with different amounts of water concentrations. Figure (8) can be compared with figure (6), for impedance representation.

Figure (9) displays the Nyquist representation of conductivity of sandclay with different amounts of gasoline concentrations (10 μ L, 20 μ L, 30 μ L, 40 μ L, 50 μ L and 60 μ L). The behavior of the samples in figure (9) can be compared with the behavior of figure (7), for impedance representation.

The water contamination decreases the whole sample impedances. The gasoline contamination increases the the whole sample impedances.

266

267 **3**) CONCLUSION

In the laboratory, conductivity of samples increases with adding water 268 concentration while with the additions of gasoline causes a conductivity to 269 decrease. Electrical conduction, in general, is raised with rise of overall 270 conductor continuous links and with frequency increase. There is a link 271 between hydrocarbons contamination and geophysical signal and the electrical 272 273 resistivity. The bulk conductivity observed in contaminated samples is linked 274 to contaminant fluid conductivity and its amount and consequently changes 275 according to the type of contaminant. So we could infer that type of contaminant is important at altering geophysical properties of contaminated 276 277 sediments. Hence, influence of type of contaminant on physical properties 278 cannot be ignored in geophysical contaminated sites. Frequency effect of 279 conductivity is reflected from orientation and translation hopping. The 280 dependence of impedance on frequency indicates distribution of relaxation in the samples. Imaginary impedance peaks are shifted to higher frequency side 281 with increase of filtered water. Finally, the electrical measurements are good 282 283 support for analysis to define qualitatively the type of contaminant.

284 **4) REFERENCES**

Abou El-Anwar E., Gomaa M. M., 2013, Electrical properties and geochemistry of carbonate rocks from the Qasr El-Sagha formation, El-Faiyum, Egypt, Geophysical Prospecting, Vol. 61, pp. 630–644.

Abou El-Anwar E., Gomaa M. M., 2016, Electrical, mineralogical, geochemical and provenance of Cretaceous black shales, Red Sea Coast, Egypt, Egyptian Journal of Petroleum, Vol. 25, pp. 323- 332.

- Barabanova E V, Malyshkina O V, Ivanova A I, Posadova E M,
 Zaborovskiy K M and Daineko A V, Effect of porosity on the electrical
 properties of PZT ceramics., Materials Science and Engineering 49 (2013)
 012026 doi:10.1088/1757-899X/49/1/012026
- Bussian A. E., 1983, Electrical conductance in a porous medium, Geophys., Vol. 48, No. 9, pp. 1258- 1268.
- Chelidze T. and Guéguen Y., 1999, Electrical spectroscopy of porous
 rocks: a review -I. Theoretical models, Geophys. J. Int., 137, 1–15.
- Chelidze T. Guéguen Y. and Ruffet C., 1999, Electrical spectroscopy of
 porous rocks: a review -II. Experimental results and interpretation, Geophys. J.
 Int., 137, 16-34.
- Chelidze T. L., 1979, A Percolation model of the electrical conductivity of
 minerals, Izvestiya, Earth Physics, Vol. 15, No. 11.pp. 849- 850.
- Chew W. C., and Sen P. N., 1982, Dielectric enhancement due to electrochemical double layer: thin double layer approximation, J. Chem. Phys., Vol. 77, No. 9, pp. 4683- 4693.
- 307 Chinh P. D., 2000, Electrical properties of sedentary rocks having
 308 interconnected water- saturated pore spaces, Geophysics, Vol. 65, No. 4, pp.
 309 1093-1097.
- Dias C. A., 2000, Development in a model to describe low- frequency electrical polarization of rocks, Geophys., Vol. 65, No. 2, pp. 437-451.

312	Garrouch A. A. and Sharma M. M., 1994, The influence of clay content,
313	Salinity, Stress, and wettability on the dielectric properties of brine- saturated
314	rocks: 10 Hz to 10 MHz, Geophys., Vol. 59, No. 6, pp. 909- 917.
315	Gomaa M. M., 2008, Relation between electric properties and water
316	saturation for hematitic sandstone with frequency, Annals of Geophysics, Vol.
317	51, No. 5/6, pp. 801-811.
318	Gomaa M. M., 2009, Saturation effect on Electrical properties of hematitic
319	sandstone in the audio frequency range using non-polarizing electrodes,
320	Geophysical Prospecting, Vol. 57, pp. 1091–1100.
321	Gomaa M. M., 2013, Forward and inverse modeling of the electrical
322	properties of magnetite intruded by magma, Egypt, Geophysical Journal
323	International, Vol. 194, Issue 3, pp. 1527-1540.
324	Gomaa M. M., Abou El-Anwar E., 2015, Electrical and geochemical
325	properties of tufa deposits as related to mineral composition in South Western
326	Desert, Egypt, Journal of Geophysics and Engineering, Vol. 12, No. 3, pp. 292-
327	302.
328	Gomaa M. M., Abou El-Anwar E., 2017, Electrical, mineralogical, and
329	geochemical properties of Um Gheig and Um Bogma Formations, Egypt,
330	Carbonates and Evaporites, pp. 1-14.
331	Gomaa M. M., Alikaj P., 2009, Effect of electrode contact impedance on a.

- c. electrical properties of wet hematite sample, Marine Geophysical researches,
- 333 Volume 30, Number 4, pp. 265-276.

Gomaa M. M., Elsayed R. M., 2006, Thermal Effect of Magma Intrusion 334 on Electrical Properties of Magnetic Rocks from Hamamat Sediments, NE 335 Desert, Egypt, presented at the 68th Conference and Exhibition incorporating 336 SPE Europe: European Association of Geoscientists and Engineers (EAGE), 337 Poster P328, Session " Gravity, Magnetics, Mining and Geothermal ", 338 Opportunities in Mature Areas 6, 12-15 June, Vienna, Austria, pp. 3550-3555. 339 340 Gomaa M. M., Elsayed R. M., 2009, Thermal Effect of Magma Intrusion 341 on Electrical Properties of Magnetic Rocks from Hamamat Sediments, NE Desert, Egypt, Geophysical Prospecting, Vol. 57, No. 1, pp. 141-149. 342 Gomaa M. M., Hussain S. A., El- Diwany E. A., Bayoumi A. E., and 343 Ghobashy M. M., 2000, Modeling of A. C. electrical properties of humid sand 344 345 and the effect of water content, Society of Exploration Geophysicists (SEG), International Exposition and 70th Annual Meeting, Calgary, Alberta, Canada, 346 19 (1), pp. 1850-1853. 347 Gomaa M. M., Kassab M., 2016, Pseudo random renormalization group 348 forward and inverse modeling of the electrical properties of some carbonate 349

rocks, Journal of Applied Geophysics, Vol. 135, pp. 144-154.

Gomaa M. M., Kassab M., 2017, Forward and inverse modelling of electrical properties of some sandstone rocks using renormalisation group method, Near Surface Geophysics, Vol. 15 (5), pp. 487- 498.

Gomaa M. M., Kassab M., El-Sayed N. A., 2015 a, Study of petrographical
and electrical properties of some Jurassic carbonate rocks, north Sinai, Egypt,
Egyptian Journal of Petroleum, Vol. 24 (3), pp. 343- 352.

Gomaa M. M., Kassab M., El-Sayed N. A., 2015 b, Study of electrical
properties and petrography for carbonate rocks in the Jurassic Formations:
Sinai Peninsula, Egypt, Arabian Journal of Geosciences, Vol. 8, Issue 7, pp.
4627-4639.

Gomaa M. M., Metwally H., Melegy A., 2018, Effect of concentration of
salts on electrical properties of sediments, Lake Quaroun, Fayium, Egypt,
Carbonates and Evaporites, pp. 1-9.

Gomaa M. M., Shaltout A., Boshta M., 2009, Electrical properties and mineralogical investigation of Egyptian iron ore deposits, Materials Chemistry and Physics, Volume 114, Issue 1, 2009, pp. 313-318.

Gomaa M.M., 2006, Interpretation of Electrical Properties for Humid and
Saturated Hematitic Sandstone Sample, presented at the 68th Conference and
Exhibition incorporating SPE Europe: European Association of Geoscientists
and Engineers (EAGE), Oral H021, Session "Gravity, Magnetics, Mining and
Geothermal", Opportunities in Mature Areas 4, 12- 15 June, Vienna, Austria,
pp. 2182-2186.

Hill R. M. and Jonscher A. K., 1983, The dielectric behavior of condensed
matter and its many- body interpretation, Contemp. Phys., Vol. 24, No. 1, pp.
75- 110.

Jonscher A. K., 1973, Carrier and matrix losses in solid dielectrics, In 1972
Annual report conference on Electrical insulation and dielectric phenomena,
(Natn: Academy of Sci., Washington D. C., 1973), pp. 418- 425.

379	Jonscher A. K., 1975, The interpretation of non- dielectric admittance and
380	impedance diagrams, Phys. Stat. Sol. (a) 32, pp. 665-675.
381	Jonscher A. K., 1977, Review article the universal dielectric response,
382	Nature, Vol. 267, pp. 673- 679.
383	Jonscher A. K., 1999, Review article Dielectric relaxation in solids, J.
384	Phys. D: Appl. Phys., Vol. 32, pp. R57- R70.
385	Kassab M., Gomaa M. M., Lala A., 2017, Relationships between electrical
386	properties and petrography of El-Maghara sandstone formations, Egypt,
387	NRIAG Journal of Astronomy and Geophysics, Vol. 6, pp.162-173.
388	Khalafalla A. S. and Maegley W. J., 1973, Low- frequency impedance

parameters of basalt, Granite, and Quartzite, Geophys., Vol. 38, No. 1, pp. 68-75.

- Knight R. J. and Abad A., 1995, Rock/ water interaction in dielectric
 properties: Experiments with Hydrophobic sandstones, Geophys., Vol. 60, No.
 2, pp. 431- 436.
- Knight R. J. and Nur A., 1987, The permittivity of sandstones, 60 kHz to 4
 MHz, Geophys., pp. 644- 654.
- Last B. J., and Thouless D. J., 1971, Percolation theory and electrical conductivity, Phys. Rev. Lett., Vol. 27, No. 25, pp. 1719- 1721.
- Leroy P., Revil A., Kemna A., Cosenza P. and Ghorbani A., 2008, Complex conductivity of water-saturated packs of glass beads, Journal of

400 Colloid and Interface Science, Volume 321, Issue 1, pp. 103-117

401 Levitskaya T. M., 1984, Dielectrical relaxation in rock, Izvestiya, Earth
402 physics, Vol. 20, No. 10, pp. 777- 780.

Levitskaya T. M., Sternberg B. K., 1996 a, Polarization processes in rocks
1. Complex dielectric permittivity method, Radio Science, vol. 31, No. 4, pp.
755-779.

Levitskaya T. M., Sternberg B. K., 1996 b, Polarization processes in rocks
2. Complex dielectric permittivity method, Radio Science, vol. 31, No. 4, pp.
781- 802.

Mendelson K. S., and Cohen M. H., 1982, The effect of grain anisotropy
on the electrical properties of sedimentary rocks, Geophys., Vol. 47, No. 2, pp.
257-263.

Minaw F., Hanna B., Mikhail F. N., 1972, Relation between the
permittivity and the dielectric loss for some Egyptian rocks, Egypt. J. Geol.,
Vol. 16, No. 2, pp. 293- 301.

415 Olhoeft G. R., 1976, electrical properties of rocks, in the physics and 416 chemistry of minerals and rocks, R. G. J. Sterns, ed., Wiley, NY. pp. 261-278.

417 Olhoeft G. R., 1977, Electrical properties of natural clay permafrost, Can.
418 J. Earth Sci., Vol. 14, pp. 16- 24.

Olhoeft G. R., 1980, Electrical properties of rocks: in Physical properties of
rocks and minerals: Touloukian Y. S., Judd W. R., & Roy R. F., Eds.,
McGrow- Hill Book Co., 257-330.

422 Olhoeft G. R., 1985, low- frequency electrical properties, Geophys., Vol.
423 50, No. 12, pp. 2492- 2503.

424	Sen P. N., 1981, Dielectric anomaly in inhomogeneous materials with
425	application to sedimentary rocks, Appl. Phys. Lett., Vol. 39, No. 8, pp. 667-
426	668.
427	Sen P. N., 1984, Short note: Grain shape effects on dielectric and electrical
428	properties of rocks, Geophys., Vol. 49, No. 5, pp. 586- 587.
429	Shaltout A. A., Gomaa M. M., Wahbe M., 2012, Utilization of standardless
430	analysis algorithms using WDXRF and XRD for Egyptian Iron Ores
431	identification, X-Ray Spectrometry, Vol. 41, pp. 355–362.
432	Song Y., Noh T. W., Lee S., & Gaines R., 1986, Experimental study of the
433	three- dimensional ac Conductivity and permittivity of a conductor- insulator
434	composite near the percolation threshold, Phys. Rev. B, Vol. 33, No. 2, pp.
435	904-908.

437	Table Caption
438	Table (1) Chemical analysis, Particle size analysis, Hydrogeological properties
439	(d _m : average diameter; K _{max} : hydraulic permeability; r: porosity).
440	Figure Caption
441	Fig (1) Displaying sample cell, where 1 is a Teflon cylinder a 2 are the two
442	electrodes enclosing the sample.
443	Fig. (2) Shows the series resistance (R_s) as a function of frequency dry and at
444	different saturations of distilled water.
445	Fig. (3) Shows the series resistance (R_s) as a function of frequency dry and at
446	different saturations of gasoline.
447	Fig. (4) Shows the permittivity (\mathcal{E}') as a function of frequency dry and at
448	different saturations of distilled water.
449	Fig. (5) Shows the permittivity (ε ') as a function of frequency dry and at
450	different saturations of gasoline.
451	Fig. (6) Shows the complex series impedance (Zs) for the sand-clay sample dry
452	and at different saturations of distilled water.
453	Fig. (7) Encloses the complex series impedance (Zp) for the sand-clay sample
454	dry and at different saturations of gasoline.
455	Fig. (8) displays the Nyquist plot of the conductivity of sand-clay as a function
456	of different amounts of water.
457	Fig. (9) displays the Nyquist plot of the conductivity of sand-clay as a function
458	of different amounts of Gasoline.















491 Fig. (7) Encloses the complex series impedance (Zp) for the sand-clay
492 sample dry and at various saturations of gasoline.



