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# In vivo calibration of esophageal pressure in the mechanically ventilated patient makes measurements reliable

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## Abstract

**Background:** Esophageal pressure (Pes) can provide information to guide mechanical ventilation in acute respiratory failure. However, both relative changes and absolute values of Pes can be affected by inappropriate filling of the esophageal balloon and by the elastance of the esophagus wall. We evaluated the feasibility and effectiveness of a calibration procedure consisting in optimization of balloon filling and subtraction of the pressure generated by the esophagus wall (Pew).

**Methods:** An esophageal balloon was progressively filled in 36 patients under controlled mechanical ventilation.  $V_{BEST}$  was the filling volume associated with the largest tidal increase of Pes. Esophageal wall elastance was quantified and Pew was computed at each filling volume. Different filling strategies were compared by performing a validation occlusion test.

**Results:** Fifty series of measurements were performed.  $V_{BEST}$  was  $3.5 \pm 1.9$  ml (range 0.5–6.0). Esophagus elastance was  $1.1 \pm 0.5$  cmH<sub>2</sub>O/ml (0.3–3.1). Both Pew and the result of the occlusion test differed among filling strategies. At filling volumes of 0.5,  $V_{BEST}$  and 4.0 ml respectively, Pew was  $0.0 \pm 0.1$ ,  $2.0 \pm 1.9$ , and  $3.0 \pm 1.7$  cmH<sub>2</sub>O ( $p < 0.0001$ ), whereas the occlusion test was satisfactory in 22 %, 98 %, and 88 % of cases ( $p < 0.0001$ ).

**Conclusions:** Under mechanical ventilation, an increase of balloon filling above the conventionally recommended low volumes warrants complete transmission of Pes swings, but is associated with significant elevation of baseline. A simple calibration procedure allows finding the filling volume associated with the best transmission of tidal Pes change and subtracting the associated baseline artifact, thus making measurement of absolute values of Pes reliable.

**Keywords:** Esophageal pressure, Pleural pressure, Transpulmonary pressure, Mechanical ventilation, Protective ventilation, Ventilator-induced lung injury, Calibration, Esophageal balloon catheter, Esophageal elastance, Esophageal artifact

## Background

Esophageal manometry has been proposed as a clinical surrogate for pleural pressure direct measurement, to guide mechanical ventilation in acute respiratory failure [1, 2]. Esophageal pressure (Pes) is currently measured by an esophageal catheter with an air-filled balloon

placed in the mid-lower portion of the esophagus. The prerequisite for using this technique is that the pressure surrounding the esophagus, i.e., the intrathoracic pressure, is correctly transmitted to the balloon. Several factors may affect the results [3, 4]. Large-size balloons, only partially inflated, are used to avoid any additional pressure due to balloon wall stretching [5, 6]. Nonetheless, due to the elastance of the esophagus wall, the filling volume was found to affect measured Pes even when the balloon is only partially inflated [5, 7]. Milic-Emili and coworkers [6] proposed two strategies to eliminate this artifact: using very

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low filling volumes ( $\leq 0.5$ – $1.0$  ml) or correcting Pes values by extrapolation to zero balloon volume. The first option, simpler, was thereafter adopted by researchers and clinicians, and discussed no further. Only recently, an in vitro study clearly demonstrated that, under positive-pressure conditions like during mechanical ventilation, very low filling volumes may be insufficient to accurately transmit both absolute values and tidal swings of Pes [8]. On the other hand, higher than traditional filling volumes result in disproportionately high Pes values, as recently reported by Chiumello and coworkers [9]. These findings support the concept that only respiratory swings of Pes are reliable, and not absolute values, thus firing up the controversy on alternative methods to compute transpulmonary pressure [10].

With the present study, we propose a new Pes calibration procedure designed to solve both the issue of low Pes transmission due to insufficient balloon filling, and the opposite issue of Pes overestimation due to significant pressure generated by the esophageal wall as a reaction to balloon filling. This procedure was tested on patients with acute respiratory failure (ARF), to evaluate its feasibility and possible advantages over traditional, not calibrated, approaches.

## Methods

We enrolled sedated and paralyzed patients with ARF under pressure-controlled mechanical ventilation, in whom an esophageal balloon catheter (Nutrivent, Sidam, Mirandola, Italy) had been inserted in the mid-lower third of the thoracic esophagus for clinical purposes. The esophageal balloon has a length of 10 cm, a nominal volume of 10 ml and a factory-recommended inflating volume of 4 ml of air. Mechanical characteristics of this catheter and other commercially available ones were previously studied in vitro [8]. Briefly, the devices were exposed to different surrounding pressures and progressively filled with air to obtain esophageal balloon pressure-volume curves. The appropriate range of filling volumes was defined by a null balloon transmural pressure and corresponded, for all the devices, to the intermediate linear section of the curve. The appropriate range was found to be catheter-specific and related to the surrounding pressure, being 0.5–8 ml for the Nutrivent catheter when the surrounding pressure was in the 0–30 cmH<sub>2</sub>O range. Appropriate catheter position was confirmed by visualization of cardiac artifacts on Pes and radiopaque markers on chest X-ray.

In each patient, we recorded the static Pes at end-expiration (Pes<sub>EE</sub>) and end-inspiration (Pes<sub>EI</sub>) while the esophageal balloon was inflated with increasing volumes from 0 to 8 ml, by 0.5-ml steps from 0 to 3 ml and 1-ml steps from 3 to 8 ml. At each volume step, the balloon was completely deflated by applying a negative pressure,

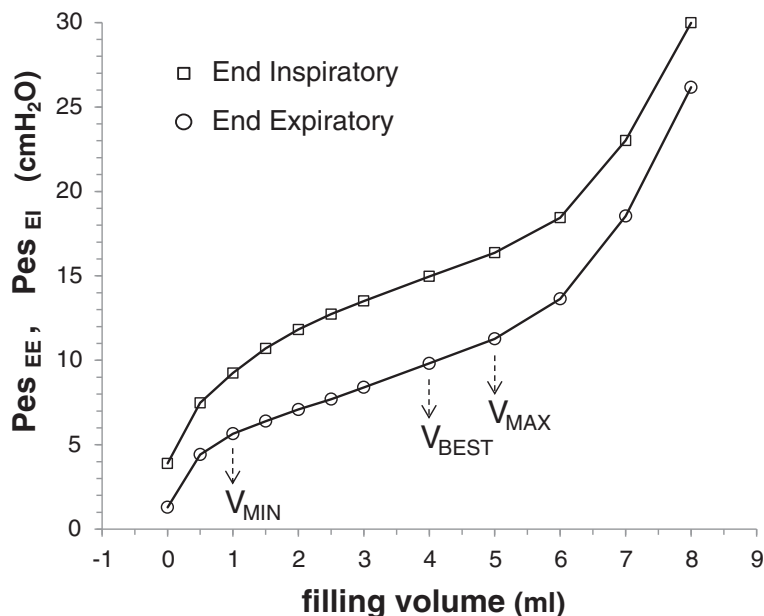
then fully inflated with 10 ml of air and finally deflated to the target volume. Static pressures were obtained by airway occlusion maneuvers of 5 s. From those data, we obtained two curves expressing the individual pressure-volume (PV) relationship between balloon filling volume and Pes, respectively at end-expiration and end-inspiration (Fig. 1).

On the end-expiratory PV curve we graphically identified the intermediate linear section and its lower and upper limits, expressed as minimum and maximum filling volumes ( $V_{MIN}$  and  $V_{MAX}$ ). According to in vitro results [8],  $V_{MIN}$  is the smaller filling volume to be injected into the esophageal catheter to pressurize it at the same level of the pressure surrounding the esophageal balloon, i.e., to reach a balloon transmural pressure of zero. Further volume injection induces progressive inflation of the esophageal balloon,  $V_{MAX}$  being the larger filling volume that does not induce overstretch of the balloon wall [8]. Therefore, the range between  $V_{MIN}$  and  $V_{MAX}$  was considered to correspond to appropriate balloon filling, with volumes below  $V_{MIN}$  denoting underfilling and volumes above  $V_{MAX}$  denoting overfilling of the balloon. Within the appropriate volume range, we identified the volume providing the maximum difference between Pes<sub>EI</sub> and Pes<sub>EE</sub> ( $V_{BEST}$ ).

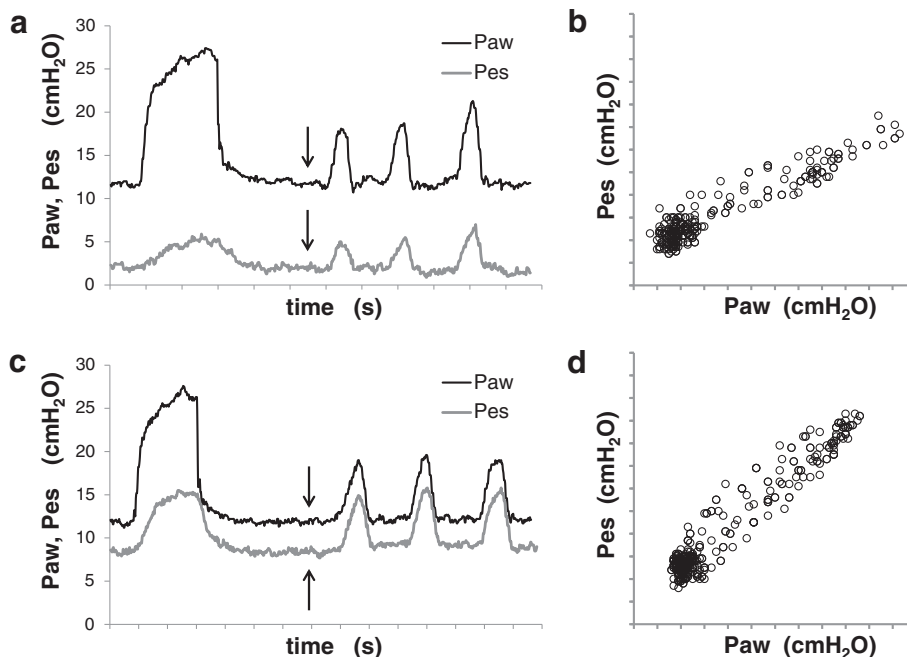
The slope of the intermediate linear section of the end-expiratory PV curve was obtained by least square fitting and it was considered to express the elastance of the esophagus (Ees) [7]. For any filling volume  $V_X$  above  $V_{MIN}$ , the pressure generated by the esophageal wall (Pew) was calculated as:  $Pew = (V_X - V_{MIN}) * Ees$  (Figure S1 in Additional file 1). Pew was considered null at filling volumes lower than  $V_{MIN}$ , the balloon transmural pressure being negative and therefore the esophagus reaction to balloon filling negligible in this case.

Then we compared five different balloon filling strategies: 0.5 ml ( $V_{0.5}$ ), as per traditional recommendations; 4.0 ml ( $V_{4.0}$ ), as per manufacturer's recommendations; 8.0 ml ( $V_{8.0}$ ), i.e., approximately at full balloon inflation; filling volume equal to individual  $V_{MIN}$ ; and filling volume equal to individual  $V_{BEST}$ . At each of these filling volumes, we measured again the static Pes<sub>EE</sub> and Pes<sub>EI</sub> and performed a validation occlusion test [3, 11]. Our patients being sedated and paralyzed, we recorded simultaneous changes of Pes ( $\Delta Pes$ ) and airway pressure (Paw) ( $\Delta Paw$ ) while applying gentle compressions on the patient's chest during an end-expiratory occlusion maneuver (Fig. 2). The hypothesis that  $V_{BEST}$  was associated with the  $\Delta Pes/\Delta Paw$  ratio closest to 1 among the different balloon filling strategies was evaluated by repeated measures ANOVA and Cochran's Q test.

From the Pes measurements obtained at a filling volume equal to individual  $V_{BEST}$  and the corresponding Pew, we computed the calibrated values of Pes (Pes<sub>CAL</sub>),



**Fig. 1** Static esophageal balloon pressure-volume curves. Relationship between balloon filling volume and static values of Pes, both at end-expiration (Pes<sub>EE</sub>, circles) and at end-inspiration (Pes<sub>EI</sub>, squares). On the end-expiratory pressure-volume (PV) curve, the intermediate linear section was graphically detected and analyzed for its lower and upper limits (V<sub>MIN</sub> and V<sub>MAX</sub>, respectively). The range between V<sub>MIN</sub> and V<sub>MAX</sub> was considered to correspond to appropriate balloon filling, with volumes below V<sub>MIN</sub> denoting underfilling and volumes above V<sub>MAX</sub> denoting overdistention. The elastance of the esophagus (cmH<sub>2</sub>O/ml) was considered equivalent to the slope of this section of the end-expiratory PV curve. Within the appropriate filling range, we identified V<sub>BEST</sub>, i.e., the filling volume associated with the maximum difference between Pes<sub>EI</sub> and Pes<sub>EE</sub>. Pes esophageal pressure



**Fig. 2** Validation test at different esophageal catheter-filling volumes. Panels (a) and (c): Paw and Pes over time, during a single mechanical respiratory breath and an end-expiratory occlusion maneuver with chest compressions. Arrows refer to the start of the occlusion maneuver. Panels (b) and (d): Pes/Paw relative changes during the end-expiratory occlusion maneuver. Panels (a) and (b) correspond to an esophageal balloon catheter filling of 0.5 ml, while panels (c) and (d): correspond to a filling of 2.5 ml. The slope of the Pes/Paw relationship was 0.48 with an injected volume of 0.5 ml (panel b) and 1.02 with an injected volume of 2.5 ml (panel d). Paw airway pressure, Pes esophageal pressure

as previously suggested [6, 7]:  $Pes_{CAL} = Pes - Pew$ . The hypothesis that  $Pes_{CAL}$  significantly differed from raw measurements of  $Pes$  at  $V_{0.5}$  ( $Pes_{V0.5}$ ),  $V_{4.0}$  ( $Pes_{V4.0}$ ) and  $V_{BEST}$  ( $Pes_{VBEST}$ ) was evaluated by Bland-Altman analysis and repeated measures ANOVA. The study was approved by the committee on research ethics at the institution in which the enrollment was conducted (Fondazione IRCCS Policlinico S. Matteo, Pavia, Italy) and informed consent was obtained as required.

## Results

Fifty series of measurements were performed in 36 patients (20 males,  $57 \pm 17$  years) undergoing pressure controlled mechanical ventilation. In nine patients, multiple measurements at different body positions and/or positive end-expiratory pressure (PEEP) settings were performed: six patients were studied twice, one patient three times and two patients four times. Body position was supine with the bed at 20–30 degrees head up, lateral and prone in 45, 3 and 2 cases respectively. Settings of pressure-controlled mechanical ventilation were: inspiratory oxygen fraction ( $FiO_2$ )  $0.71 \pm 0.22$ , PEEP  $11.8 \pm 5.0$  cmH<sub>2</sub>O, peak pressure  $28.6 \pm 5.5$  cmH<sub>2</sub>O, respiratory rate  $15.7 \pm 5.2$  bpm. Tidal volume/ideal body weight was  $7.9 \pm 1.8$  ml/kg, plateau pressure  $27.6 \pm 5.0$  cmH<sub>2</sub>O and partial pressure of oxygen in arterial blood ( $PaO_2$ )/ $FiO_2$  ratio  $165 \pm 76$  mmHg. Causes of acute respiratory failure were: community-acquired pneumonia (7), heart failure (2), chronic obstructive pulmonary disease (COPD) decompensation (1), acute respiratory distress syndrome (ARDS) (7), abdominal compartment syndrome (6), pulmonary alveolar proteinosis (8), and postoperative respiratory complications (5). Pulmonary alveolar proteinosis patients were studied during the whole lung lavage procedure previously described [12]. In five patients, body mass index was higher than 50 kg/m<sup>2</sup>.

### Esophageal balloon pressure-volume curves in mechanically ventilated patients

End-expiratory and end-inspiratory complete esophageal balloon PV curves were obtained in all cases; in some patient, filling volumes larger than 6 ml stimulated esophageal peristaltic contractions that were rapidly self-limiting. An intermediate linear section of the end-expiratory esophageal balloon PV curve was graphically detected in all cases. Lower and upper limit of this section, i.e.,  $V_{MIN}$  and  $V_{MAX}$ , were  $1.5 \pm 0.6$  and  $5.4 \pm 0.9$  cmH<sub>2</sub>O, respectively.  $V_{MIN}$  ranged from 0.0 to 3.0 ml and its value directly correlated with  $Pes_{EE}$  ( $r = 0.766$ , 95 % CI 0.620 to 0.861;  $p < 0.0001$ ). Mean value of  $V_{BEST}$  was  $3.5 \pm 1.9$  ml (range 0.5–6.0).  $V_{BEST}$  directly correlated with  $Pes_{EI}$  ( $r = 0.528$ , 95 % CI 0.292 to 0.703;  $p < 0.0001$ ). The slope of the linear section of the curve, i.e., the esophageal elastance (Ees), was  $1.1 \pm 0.5$  cmH<sub>2</sub>O/ml (range 0.3–3.1).

Ees was higher in females than in males ( $1.3 \pm 0.6$  vs.  $1.0 \pm 0.4$  cmH<sub>2</sub>O/ml;  $p = 0.04$ ) and was negatively correlated with body mass index ( $r = -0.629$ , 95 % CI -0.772 to -0.426;  $p < 0.0001$ ).

Figure 3 shows representative end-expiratory and end-inspiratory static esophageal balloon pressure-volume curves obtained in four different patients. Figure S2 in Additional file 1 shows the average end-expiratory and end-inspiratory esophageal balloon pressure-volume curves, and Figure S3 in Additional file 1 shows three end-expiratory static esophageal balloon pressure-volume curves obtained at three different PEEP levels in the same patient.

### Effects of balloon inflation on pressure transmission and esophageal wall pressure

$Pes_{EE}$  and  $Pes_{EI}$  progressively increased with the increase of balloon filling volume ( $p < 0.0001$ ).  $\Delta Pes$  was  $5.3 \pm 2.3$  cmH<sub>2</sub>O at  $V_{BEST}$  and it was decreased by 7 %, 17 %, 17 %, and 39 % when the balloon was filled at  $V_{4.0}$ ,  $V_{MIN}$ ,  $V_{8.0}$ , and  $V_{0.5}$  respectively ( $p < 0.0001$ ). The  $\Delta Pes/\Delta Paw$  ratio closest to 1 was observed at  $V_{BEST}$  ( $0.96 \pm 0.06$ ;  $p < 0.0001$  vs. all the other filling strategies).  $\Delta Pes/\Delta Paw$  ratio was in the 0.8–1.2 range in 98 %, 88 %, 64 %, 60 %, and 22 % of cases when the balloon was inflated at  $V_{BEST}$ ,  $V_{4.0}$ ,  $V_{MIN}$ ,  $V_{8.0}$ , and  $V_{0.5}$  respectively ( $p < 0.001$ ). At  $V_{BEST}$   $Pew$  was  $2.0 \pm 1.9$  cmH<sub>2</sub>O (range 0.0–6.0). These findings are summarized in Table 1 and Fig. 4.

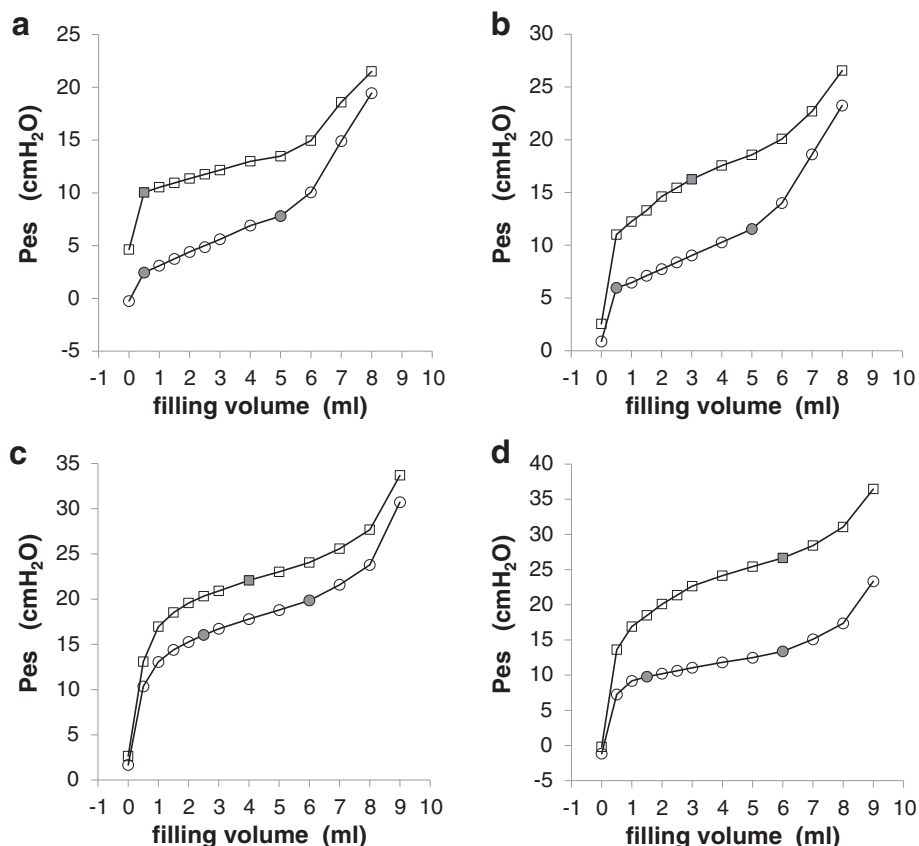
### Calibration procedure

Considering end-expiratory and end-inspiratory conditions all together, mean value of  $Pes_{CAL}$  was  $13.0 \pm 5.9$  cmH<sub>2</sub>O; compared to  $Pes_{CAL}$ ,  $Pes_{V0.5}$  was significantly lower ( $9.0 \pm 4.0$  cmH<sub>2</sub>O;  $p < 0.0001$ ), whereas  $Pes_{V4.0}$  ( $15.9 \pm 5.1$  cmH<sub>2</sub>O;  $p < 0.0001$ ) and  $Pes_{VBEST}$  ( $15.1 \pm 6.0$  cmH<sub>2</sub>O;  $p < 0.0001$ ) were significantly higher. Bland-Altman analyses are shown in Fig. 5 and in Figure S4 of Additional file 1.

## Discussion

We evaluated esophageal manometry in patients with ARF under positive-pressure mechanical ventilation. Our main findings are:

1. The optimal filling volume of the esophageal balloon ( $V_{BEST}$ ) can be easily identified as the one that maximizes respiratory  $\Delta Pes$ .
2. The value of  $V_{BEST}$  varies in a large range, typically is much larger than traditionally used small filling volumes, and thus is frequently associated with a significant esophageal wall pressure ( $Pew$ ).
3. A simple calibration procedure, based on balloon filling at  $V_{BEST}$  and subtracting the associated  $Pew$ , allows improvement of the assessment of both relative changes and absolute values of  $Pes$ .



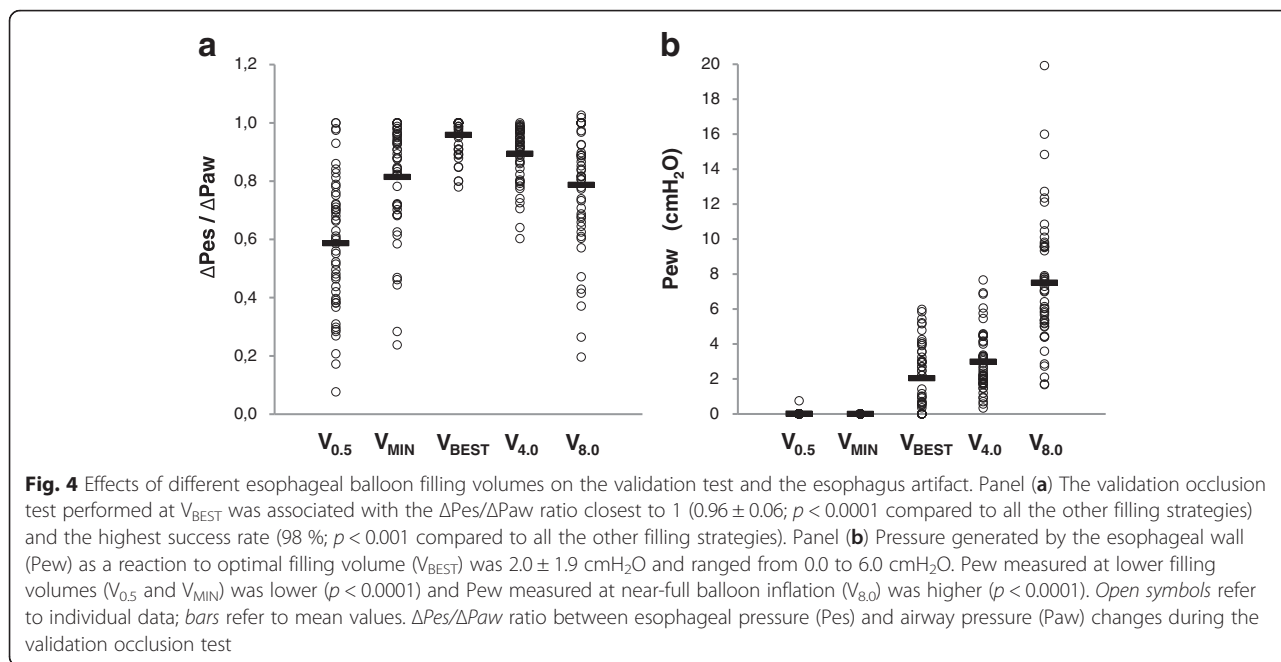
**Fig. 3** Examples of inspiratory and expiratory static esophageal pressure-volumes curves. *Circles* refer to end-expiratory esophageal pressure ( $P_{esEE}$ ); *closed circles* refer to  $V_{MIN}$  and  $V_{MAX}$  as graphically detected (respectively lower and upper limits of the intermediate linear section of the curve). *Squares* refer to end-inspiratory esophageal pressure ( $P_{esEI}$ ); *closed squares* refer to  $V_{BEST}$  (the filling volume associated with the largest  $P_{esEI} - P_{esEE}$  difference). Panel (a) 32-year-old male patient, body mass index (BMI) 27 kg/m<sup>2</sup>; pulmonary alveolar proteinosis and kyphoscoliosis; positive end-expiratory pressure (PEEP) 0 cmH<sub>2</sub>O; tidal volume (TV) 550 ml, plateau pressure (Pplat) 20 cmH<sub>2</sub>O.  $V_{MIN}$  and  $V_{BEST}$  0.5 ml. Esophageal elastance 1.3 cmH<sub>2</sub>O/ml, pressure generated by the esophageal wall ( $P_{ew}$ ) at  $V_{BEST}$  0.0 cmH<sub>2</sub>O. Panel (b) 82-year-old female patient, BMI 22 kg/m<sup>2</sup>; respiratory failure after pulmonary endarterectomy; PEEP 7 cmH<sub>2</sub>O, TV 500 ml, Pplat 25 cmH<sub>2</sub>O.  $V_{MIN}$  0.5 ml and  $V_{BEST}$  3 ml. Esophageal elastance 1.3 cmH<sub>2</sub>O/ml,  $P_{ew}$  at  $V_{BEST}$  3.3 cmH<sub>2</sub>O. Panel (c) 31-year-old male patient, BMI 63 kg/m<sup>2</sup>; legionella pneumonia and morbid obesity; PEEP 12 cmH<sub>2</sub>O, TV 450 ml, Pplat 30 cmH<sub>2</sub>O.  $V_{MIN}$  2.5 ml and  $V_{BEST}$  4.0 ml. Esophageal elastance 1.2 cmH<sub>2</sub>O/ml,  $P_{ew}$  at  $V_{BEST}$  1.8 cmH<sub>2</sub>O. Panel (d) 70-year-old male patient, BMI 23 kg/m<sup>2</sup>; intra-abdominal hypertension due to large retroperitoneal hematoma; PEEP 10 cmH<sub>2</sub>O, TV 370 ml, Pplat 29 cmH<sub>2</sub>O.  $V_{MIN}$  1.5 ml and  $V_{BEST}$  6 ml. Esophageal elastance 0.8 cmH<sub>2</sub>O/ml,  $P_{ew}$  at  $V_{BEST}$  3.6 cmH<sub>2</sub>O.  $P_{es}$  esophageal pressure

**Table 1** Esophageal pressure measurements in patients under positive-pressure ventilation with five different esophageal balloon filling strategies

	Volume (ml)	$P_{esEE}$ (cmH <sub>2</sub> O)	$P_{esEI}$ (cmH <sub>2</sub> O)	$\Delta P_{es}$ (cmH <sub>2</sub> O)	$\Delta P_{es}/\Delta P_{aw}$	$P_{ew}$ (cmH <sub>2</sub> O)
$V_{0.5}$	0.5 ± 0.0*	7.3 ± 3.6*	10.6 ± 3.8*	3.3 ± 1.9 <sup>£</sup>	0.59 ± 0.23 <sup>£</sup>	0.0 ± 0.1 <sup>^</sup>
$V_{MIN}$	1.5 ± 0.6*	10.4 ± 5.2*	14.8 ± 5.7*	4.4 ± 2.0 <sup>§</sup>	0.81 ± 0.19 <sup>§</sup>	0.0 ± 0.0 <sup>^</sup>
$V_{BEST}$	3.5 ± 1.9 <sup>#</sup>	12.5 ± 5.2 <sup>#</sup>	17.8 ± 5.6 <sup>#</sup>	5.3 ± 2.3*	0.96 ± 0.06*	2.0 ± 1.9 <sup>#</sup>
$V_{4.0}$	4.0 ± 0.0 <sup>#</sup>	13.4 ± 4.4 <sup>#</sup>	18.4 ± 4.7 <sup>#</sup>	4.9 ± 2.1 <sup>§</sup>	0.89 ± 0.10 <sup>§</sup>	3.0 ± 1.7 <sup>#</sup>
$V_{8.0}$	8.0 ± 0.0*	23.8 ± 6.5*	28.2 ± 6.1*	4.4 ± 2.4 <sup>§</sup>	0.79 ± 0.21 <sup>§</sup>	7.5 ± 3.6*

$P_{esEE}$ ,  $P_{esEI}$  and  $\Delta P_{es}$  end-expiratory, end-inspiratory, and tidal swing of  $P_{es}$  respectively,  $\Delta P_{es}/\Delta P_{aw}$  esophageal to airway pressure change ratio during an occlusion test (airway opening occlusion and chest compressions),  $P_{ew}$  pressure generated by the esophageal wall as a reaction to balloon volume increase,  $V_{0.5}$ ,  $V_{4.0}$  and  $V_{8.0}$  injected volumes of 0.5, 4, and 8 ml respectively,  $V_{MIN}$  lower limit of the linear section of the end-expiratory PV curve,  $V_{BEST}$  injected volume associated with the largest  $P_{es}$  swing (see Methods and Fig. 1 for details)

\*  $p < 0.0001$  vs. all the other injected volumes; #  $p < 0.0001$  vs.  $V_{0.5}$ ,  $V_{MIN}$ , and  $V_{8.0}$ ; ^  $p < 0.0001$  vs.  $V_{4.0}$ ,  $V_{8.0}$ , and  $V_{BEST}$ ; §  $p < 0.0001$  vs.  $V_{0.5}$  and  $V_{BEST}$ ;  $p < 0.05$  vs.  $V_{8.0}$  and  $V_{MIN}$ ;  $p < 0.0001$  vs.  $V_{0.5}$  and  $V_{BEST}$ ;  $p < 0.05$  vs.  $V_{4.0}$ ;  $p < 0.0001$  vs.  $V_{MIN}$ ,  $V_{BEST}$ , and  $V_{4.0}$ ;  $p < 0.05$  vs.  $V_{8.0}$

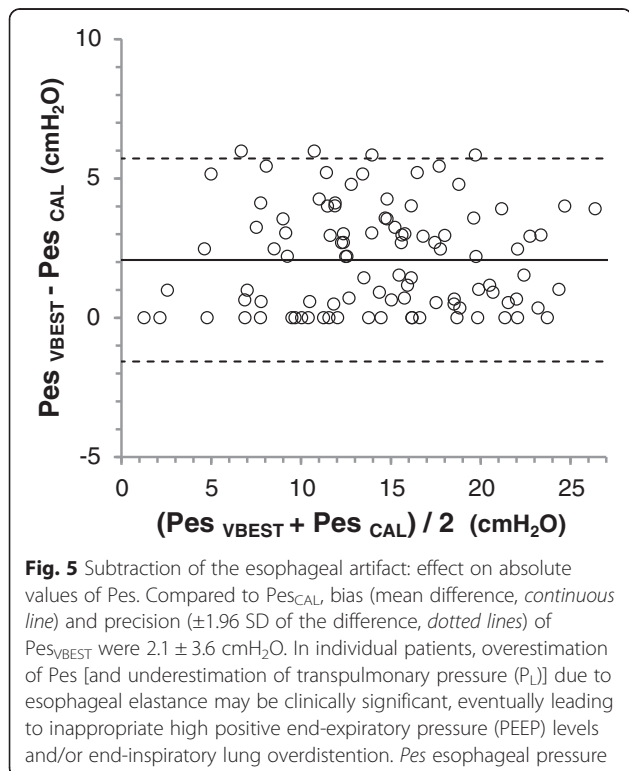


Esophageal pressure is used as surrogate for pleural pressure (Ppl) in order to compute transpulmonary (airways minus pleural) pressure ( $P_L$ ), i.e., the effective pressure distending the lung parenchyma. Ideally, in mechanically ventilated patients we should maintain positive values of  $P_L$  at end-expiration while avoiding

excessive  $P_L$  at end-inspiration, to limit both lung derecruitment and overdistention. These theoretical assumptions were recently translated into two different practical approaches to set PEEP, with potential advantages in ARF [1, 2]. The two approaches are based on different methods to compute transpulmonary pressure: Talmor and colleagues assumed the absolute value of esophageal pressure to be equal to pleural pressure (direct method), whereas Grasso and colleagues computed pleural pressure by partitioning airway pressure according to respiratory swings of esophageal pressure (elastance-derived method).

It was recently demonstrated that, under positive-pressure conditions, the use of traditional small filling volumes is associated with underfilling and thus malfunctioning of the esophageal balloon catheter in most cases [8]. Underfilling involves under-transmission of both absolute values and respiratory swings of esophageal pressure, and therefore may affect both the direct and the elastance-derived method.

In this study in patients with ARF under controlled mechanical ventilation, the minimum filling volume ( $V_{MIN}$ ) that was able to accurately transmit the end-expiratory esophageal pressure was substantially larger than 0.5 ml in most cases, being on average 1.5 ml and reaching values as high as 3 ml. As previously observed in vitro [8], the in vivo  $V_{MIN}$  was proportional to the surrounding pressure: the higher the Pes, the larger the volume to be injected into the catheter. Moreover, the filling volume providing optimal transmission of Pes respiratory swings ( $V_{BEST}$ ) was substantially larger than  $V_{MIN}$ , being on average 3.5 ml and directly related to the Pes value. The positive relationship between  $V_{BEST}$  and Pes is



explained by the fact that part of the volume injected into the esophageal catheter must be spent to pressurize the system at the pressure level surrounding the balloon. The dynamic occlusion test is the classic method to validate a  $P_{es}$  measurement [3, 11]: similar  $P_{es}$  and  $P_{aw}$  swings should be observed during spontaneous respiratory efforts (or manual chest compressions in the case of a passive patient) against the closed airway opening. A major finding of our study is that in almost all cases the balloon filling volume required to pass the validation occlusion test was much larger than 0.5 ml. Therefore we suggest abandoning the systematic use of the “traditional” small filling volumes. A simple option could be to use a fixed higher filling volume. However,  $V_{BEST}$  was highly variable among different patients and conditions, ranging from 0.5 to 6 ml in our series. This suggests that the esophageal catheter filling volume should be adapted to the intrathoracic pressure condition of any given patient. Therefore, in order to obtain reliable esophageal pressure waveforms, we suggest filling the esophageal balloon catheter progressively step-by-step and selecting, within the catheter-specific range of filling volumes [8], the volume associated with the largest esophageal pressure tidal swing. Since dynamic and static tidal variation of  $P_{es}$  are very similar [13], for clinical purposes the procedure can be performed without occlusion maneuvers at each filling step. Many factors, like mechanical ventilation setting, body position, fluid balance and intra-abdominal pressure, can influence intrathoracic pressure in critically ill patients. At any significant change of one or more of these factors, for better results the optimal filling volume of the esophageal balloon catheter should be rechecked.

The use of larger filling volumes stimulated significant esophageal reaction in our patients. The pressure generated by the esophageal wall, when progressively distended, has both a passive (collagen and elastic fibers) and an active (smooth muscle tone) component, as well described by Orvar and colleagues [14]. When a balloon was progressively inflated in the esophagus of awake healthy volunteers, the pressure generated by the esophageal wall ( $P_{ew}$ ) was linearly related to the esophageal cross-sectional area (CSA): for each 10 mm<sup>2</sup> increase in CSA above 50 mm<sup>2</sup>,  $P_{ew}$  increased by 1 cmH<sub>2</sub>O. Thresholds for peristaltic contractions and for pain or pressure sensation were 150 and 300 mm<sup>2</sup> respectively. The esophageal catheter we used is a nasogastric tube (20 mm<sup>2</sup> CSA) provided with a 10-cm-long esophageal balloon that reaches 180 mm<sup>2</sup> CSA when fully inflated with approximately 10 ml. Therefore, a detectable  $P_{ew}$  was expected at intermediate balloon filling volumes (but not in case of deflated or minimally inflated balloon), whereas peristaltic contractions were expected only for higher filling volumes, approximating full balloon inflation. On average we observed a  $P_{ew}$  of about 1 cmH<sub>2</sub>O for each milliliter of

injected volume above  $V_{MIN}$ . When  $V_{BEST}$  was injected into the catheter,  $P_{ew}$  was 2 cmH<sub>2</sub>O on average and reached values as high as 6 cmH<sub>2</sub>O. With a balloon near fully inflated,  $P_{ew}$  was about 8 cmH<sub>2</sub>O on average with single values as high as 20 cmH<sub>2</sub>O. This esophageal reaction to balloon inflation is a well-known artifact affecting absolute values of esophageal pressure, which may therefore become substantially more positive than pleural pressure [5, 7]. Such an artifact can result in significant and unpredictable overestimation of  $P_{es}$  and underestimation of  $P_{L}$ , possibly leading to inappropriately high PEEP levels and/or end-inspiratory lung overdistention when a  $P_{es}$ -guided mechanical ventilation strategy is adopted. Our data suggest that the risk overestimation of  $P_{es}$  is higher in case of female subjects and/or moderate-low body mass indexes. These findings are consistent with gender differences in the responses to esophageal balloon distention [15] and high prevalence of hypomotility of the esophageal body in obese patients [16]. Milic-Emili and colleagues [6] suggested using very small filling volumes for the esophageal balloon in order to easily minimize the esophageal artifact and their recommendation survived for about 50 years, being only recently rediscovered [3, 8]. Our findings prove that, in mechanically ventilated ARF patients, it is not possible to avoid balloon underfilling and esophageal artifact at the same time. This technical dilemma may explain why different research groups obtained low [17], moderate [18, 19] or high [9] absolute  $P_{es}$  values in the same condition of supine subjects at functional residual capacity.

To solve this technical problem, we reconsidered and adapted a procedure originally proposed by Milic-Emili who suggested – as an alternative to small filling volumes – to extrapolate to zero balloon volume the  $P_{es}$  measured at higher filling volumes [6]. Our calibration procedure significantly improved the quality of  $P_{es}$  measurement. Tidal swings of  $P_{es}$  were maximized, thus allowing passing of the validation test in almost all cases. Moreover, it was possible to recognize and subtract from  $P_{es}$  the pressure generated by the esophageal wall, which would have significantly raised  $P_{es}$  above the pleural value. In our opinion, calibrated  $P_{es}$  represents the best surrogate for absolute pleural pressure in critical care patients and may significantly improve the direct method proposed by Talmor and colleagues [1].

#### Limitations of the study

Since we did not obtain direct measurements of pleural pressure in our patients, our statement that calibrated  $P_{es}$  reflects  $P_{pl}$  better than uncalibrated  $P_{es}$  is based on the reasonable assumption that the removal of artifacts should improve a measure. Our calibration procedure was designed according to general principles and therefore for application to different esophageal catheters.

However, the study was performed with a single specific esophageal balloon catheter and therefore the results cannot be straightly generalized. Esophageal balloon catheters of different manufacturers show a very similar behavior when progressively inflated under positive-pressure conditions, the major difference among devices being the amplitude of appropriate filling volumes range [8]. The catheter used in the present study is a nasogastric tube provided with a large esophageal balloon with a wide range of appropriate filling volumes. With different esophageal catheters we should expect different optimal filling volumes, different esophageal reaction, and therefore different calibration factors. We studied passive patients under controlled mechanical ventilation: the feasibility of our calibration procedure in active patients should be verified. In particular, during assisted spontaneous breathing, the variability of end-expiratory lung volume might prevent the correct computation of esophageal elastance, while the variability of tidal volume might make detection of optimal filling volume more difficult.

## Conclusions

The present study demonstrates that an approach based on a calibrated esophageal pressure is feasible and provides significant improvement of the technique over traditional approaches. Clinical advantages of using a calibrated esophageal pressure to guide mechanical ventilation should be demonstrated by future trials.

## Key messages

- Esophageal pressure measurement can be affected by inappropriate balloon filling and esophageal elastance.
- In mechanically ventilated patients, traditional small filling volumes are almost always inappropriate.
- Optimal filling volume within the catheter-specific appropriate range is easy to find as the one that maximizes respiratory  $\Delta$ Pes.
- The pressure generated by the esophagus wall as a reaction to optimal balloon filling may significantly affect Pes.
- In vivo calibration of Pes, by selecting the optimal balloon filling and subtracting the esophagus artifact, makes Pes-guided mechanical ventilation more reliable.

## Additional file

**Additional file 1 Figure S1.** In vitro and in vivo Pressure-Volume curves of the esophageal balloon. Within the intermediate linear section of the

esophageal balloon PV curve, Pes is stable when the balloon is inflated in vitro (dotted line), whereas Pes linearly increases with the increase of the filling volume in vivo (open circles) due to esophageal elastance (Ees). When pressure generated by the esophageal wall is subtracted from Pes (Pes-Pew; closed circles), in vitro and in vivo curves closely parallel each other. Dotted line: in vitro PV curve obtained by progressive inflation of the balloon while the surrounding pressure was maintained at 10 cmH<sub>2</sub>O. Open circles: end-expiratory PV curve obtained in a patient under controlled mechanical ventilation with high positive end-expiratory pressure (15 cmH<sub>2</sub>O). Closed circles: end-expiratory PV curve obtained by subtraction of Pew from raw Pes values in the same patient. **Figure S2.** Average end-expiratory and end-inspiratory esophageal balloon pressure-volume curves in acute respiratory failure patients. Open circles: end-expiratory static Pes values (Pes<sub>EE</sub>); open squares: end-inspiratory static Pes values (Pes<sub>EI</sub>). Vertical lines refer to standard deviation of Pes. Horizontal lines refer to standard deviation of specific filling volumes detected on the esophageal balloon pressure-volume curves (V<sub>MIN</sub>, V<sub>BEST</sub> and V<sub>MAX</sub>). V<sub>0.5</sub> was lower than V<sub>MIN</sub>, i.e. it was associated to balloon underfilling at end-expiration, in 42 cases (84 %); V<sub>0.5</sub> was lower than V<sub>BEST</sub>, i.e. it was associated to suboptimal  $\Delta$ Pes in 47 cases (94 %). V<sub>MIN</sub> was lower than V<sub>BEST</sub> in 37 cases (74 %), being the V<sub>BEST</sub> - V<sub>MIN</sub> difference 2.0  $\pm$  1.7 ml. **Figure S3.** End-expiratory static esophageal balloon pressure-volume curves at different PEEP levels. In panel A, raw Pes values are presented; in panel B, the pressure generated by the esophageal wall (Pew) is subtracted from Pes value. Circles: ZEEP; squares: PEEP 5 cmH<sub>2</sub>O; triangles: PEEP 15 cmH<sub>2</sub>O. Closed symbols refer to V<sub>BEST</sub>, i.e. the balloon filling volume corresponding to the largest respiratory  $\Delta$ Pes (not displayed in figure). In the same patient, at increasing level of PEEP, a progressively larger balloon filling volume is needed to optimize respiratory  $\Delta$ Pes. Optimal filling volume (V<sub>BEST</sub>) stimulates a variable esophageal pressure reaction, confounding Pes measurement. For example, by filling the esophageal balloon with 5 ml, corresponding to V<sub>BEST</sub> at PEEP 15 cmH<sub>2</sub>O, raw Pes values at the three PEEP levels are very similar (panel A). Once the pressure generated by the esophageal wall is subtracted from Pes values, the PEEP-induced increase of the pressure surrounding the esophagus becomes clearly detectable (Panel B). **Figure S4.** Pes measured with traditional low filling volume (V<sub>0.5</sub>) or with manufacturer's recommended filling volume (V<sub>4.0</sub>) compared to calibrated Pes. Panel A. Compared to calibrated Pes, bias and precision ( $\pm$  1.96 SD) of Pes<sub>V0.5</sub> were -4.1  $\pm$  5.5 cmH<sub>2</sub>O. The Pes<sub>0.5</sub> - Pes<sub>CAL</sub> difference inversely correlated with the Pes<sub>0.5</sub> - Pes<sub>CAL</sub> mean value (R= -0.694, p<0.0001): the higher the Pes value, the higher the Pes underestimation due to balloon underfilling. Panel B. Compared to calibrated Pes, bias and precision ( $\pm$  1.96 SD) of Pes<sub>V4.0</sub> were -2.9  $\pm$  3.3 cmH<sub>2</sub>O. The Pes<sub>4.0</sub> - Pes<sub>CAL</sub> difference inversely correlated with the Pes<sub>4.0</sub> - Pes<sub>CAL</sub> mean value (R= -0.470, p<0.0001): the lower the Pes value, the higher the Pes overestimation due to the esophageal reaction to balloon inflation at 4 ml. (PDF 424 kb)

## Abbreviations

$\Delta$ Pes: respiratory increase of static Pes (Pes<sub>EI</sub> - Pes<sub>EE</sub>);  $\Delta$ Pes/ $\Delta$ Paw: ratio between Pes and Paw changes during the validation occlusion test; ARF: acute respiratory failure; CSA: cross-sectional area; Ees: esophagus elastance; FiO<sub>2</sub>: inspiratory oxygen fraction; Paw: airway pressure; PEEP: positive end-expiratory pressure; Pes: esophageal pressure; Pes<sub>CAL</sub>: calibrated value of Pes; Pes<sub>EE</sub> and Pes<sub>EI</sub>: static end-expiratory and end-inspiratory Pes; Pes<sub>V0.5</sub>, Pes<sub>V4.0</sub>, Pes<sub>V8.0</sub>, Pes<sub>VMIN</sub>, Pes<sub>VBEST</sub>: Pes measured with esophageal catheter filling volumes of 0.5 ml, 4 ml, 8 ml, V<sub>MIN</sub> and V<sub>BEST</sub> respectively; Pew: pressure generated by the esophagus wall as a reaction to balloon filling; P<sub>L</sub>: transpulmonary pressure; Ppl: pleural pressure; PV curve: pressure-volume curve; V<sub>0.5</sub>, V<sub>4.0</sub> and V<sub>8.0</sub>: injected volumes of 0.5, 4 and 8 ml respectively; V<sub>BEST</sub>: injected volume associated with the largest  $\Delta$ Pes; V<sub>MIN</sub> and V<sub>MAX</sub>: injected volumes corresponding to the lower and the upper limits of the linear section of the end-expiratory esophageal balloon PV curve.

## Competing interests

F. Mojoli and A. Braschi were involved in a university research spin-off for the development of NutriVent. They did not receive any payment for writing or contributing to the report. All other authors have no competing interests to declare.



**Authors' contributions**

MF contributed to study conception and design, acquisition, analysis and interpretation of data; he was involved in drafting and revising the manuscript, and gave final approval of the version to be published. IGA contributed to study conception and design, analysis and interpretation of data; he was involved in drafting and revising the manuscript, and gave final approval of the version to be published. TF contributed to acquisition, analysis and interpretation of data; she was involved in drafting the manuscript and gave final approval of the version to be published. PM contributed to study conception and design, acquisition, analysis and interpretation of data; he was involved in revising the manuscript and gave final approval of the version to be published. VCA contributed to study conception and design; he was involved in revising the manuscript and gave final approval of the version to be published. BS contributed to acquisition, analysis and interpretation of data; she was involved in drafting the manuscript and gave final approval of the version to be published. BA contributed to study conception and design; he was involved in revising the manuscript and gave final approval of the version to be published. BL contributed to study conception and design; he was involved in drafting and revising the manuscript, and gave final approval of the version to be published. All authors meet all authorship requirements. We confirm that this manuscript is not under evaluation by editors of other scientific papers.

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